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A GENERAL PROCEDURE FOR OBTAINING VELOCITY VECTOR FROM A SYSTEM--ETC(U)

JUL 79 D ADLER, R P SHREEVE

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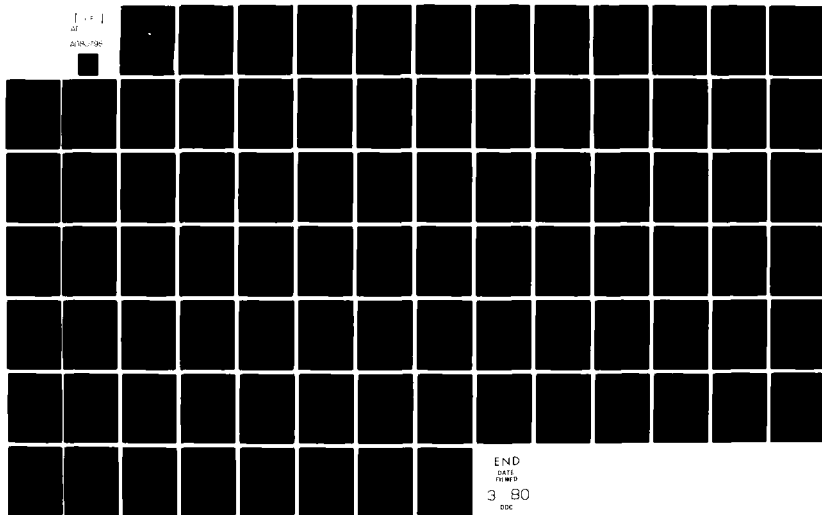
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A General Procedure for Obtaining Velocity
Vector from a System of High Response Impact
Pressure Probes

D. Adler and R. P. Shreeve

July 1979

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A technique to measure a high frequency, repetitively pulsating flow field is presented. Two impact tube probes and a Kiel probe, all with pressure transducers mounted in their tips are used. Five readings are required to identify a velocity vector at a point.

In this report the technique, the numerical procedure and the computer program used are described.

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Vector From a System of High Response Impact Pressure Probes

D. Adler and R. P. Shreeve

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Notation

- C_p - Pressure coefficient defined in eq. (3)
 α - Yaw angle relative to laboratory space
 ϕ - Pitch angle relative to laboratory space
 P_t - Total pressure
 P_s - Static Pressure
 α_{rp} - Yaw angle relative to probe axis
 ϕ_{rp} - Pitch angle relative to probe axis
 P_p - Pressure indicated by the probe
 α_p - Yaw setting of the probe
 ϕ_p - Pitch setting of the probe

Subscripts

- I }
II } relating to probe positions shown
III } in figure 3
IV }
- A relating to A type probe
B relating to B type probe
Lo lowest value in an array
rp relative to the probe axis
Up highest value in an array

Notation of PENPTS

- DD - denominator in the subsequent line of the program
- HT - penetration height (Cp of a calibration surface)
- IR - a flag with a value of either 1 or 2 to identify first or second penetration point. This flag also controls return of values to calling program or subroutine
- IB - a flag indicating the location of the last rectangle in the band checked for a penetration point. It prevents repetition of the scanning in the 103 Do loop
- NX - number of X values in the calibration surface grid (∞ values of the calibration surface)
- NY - number of Y values in the calibration surface grid (∞ values of the calibration surface)
- X(I) - X values in the grid
- XM - value of X at point B (fig. 5)
- XR(I) - two values of X returned by the subroutine as results
- XS - currently calculated value of X which is the present result and is later stored in XR(I)
- Y(J) - Y values in the calibration grid
- YC - intermediate value used in the subsequent line of the program
- YG - the Y position of the penetrating line*
- Z(I,J)- Values of the Z = Cp calibration surface above grid points
- ZX - value of Z either at point A or point C (see figs. 5, 6 and 7)
- ZM - value of Z at point B

* It should be pointed out here that the penetrating line is parallel to the X axis at a height $HT = C_p$ above the X,Y plane and at a distance YG from the X axis on the X,Y plane

Notation of INTSCS

AA	- constant defined in eq. 8
AB	- constant defined in eq. 9
ARIN	- ordinate at which scanning starts
ARLO	- lowest ordinate of calibration surface (as a condition it must be identical for all calibration surfaces used)
ARM1	- ordinate measured relative to probe 1 (the probe belonging to the first curve $C_p = \text{const.}$)
ARM2	- ordinate measured relative to probe 2 (the probe belonging to the second curve $C_p = \text{const.}$)
ARP1	- setting ordinate of probe 1
ARP2	- setting ordinate of probe 2
ARRES (1)	- abscissa value returned to INTSCS from PENPTS
ARUP	- highest ordinate of calibration surface (as a condition it must be identical for all calibration surfaces used)
AR2R	- ordinate relative to laboratory space
AR2RJ	- ordinate relative to laboratory space of previous scan
BA	- constant defined in eq. 8
BB	- constant defined in eq. 9
DAR	- ordinate step for scanning
HT1	- penetration height of calibration surface of probe 1 (C_p of probe 1)
HT2	- penetration height of calibration surface of probe 2 (C_p of probe 2)
IEPS	- a flag which is equal to 2 when the calculation is carried out as shown in fig. 11, otherwise it is equal to 1. (This information is required in the main program and is returned to it)

ISL - a flag which is equal to 10 if one of the left hand side results returned from PENPTS is 1000.0 (i.e., is not a penetration point). Otherwise it is equal to 1

ISR - a flag which is equal to 10 if one of the right hand side results returned from PENPTS is 1000.0 (i.e., is not a penetration point). Otherwise it is equal to 1

K - a flag indicating whether the first or the second intersection is evaluated

N1 - number of abscissas in calibration surface grid (fig. 4)

N2 - number of Ordinates in calibration surface grid (fig. 4)

RES1(K) - evaluated and returned abscissa of intersection

RES2(K) - evaluated and returned ordinate of intersection

R1 - radius in fig. 11 for probe 1

R2 - radius in fig. 11 for probe 2

RAIL - abscissa of point AIL in fig. 9 or 10

RAIR - abscissa of point AIR in fig. 9 or 10

RAJL - abscissa of point AJL in fig. 9 or 10

RAJR - abscissa of point AJR in fig. 9 or 10

RBIL - abscissa of point BIL in fig. 9 or 10

RBIR - abscissa of point BIR in fig. 9 or 10

RBJL - abscissa of point BJL in fig. 9 or 10

RBJR - abscissa of point BJR in fig. 9 or 10

X1(I) - abscissas of calibration surface of probe 1 or its transformation as determined by calling statement in main program

X2(I) - abscissas of calibration surface of probe 2 or its transformation as determined by calling statement in main program

- X3(I) - abscissas of calibration surface of probe 1 or its transformation as determined by calling statement in main program
- X4(I) - abscissas of calibration surface of probe 2 or its transformation as determined by calling statement in main program
- Y1(I) - ordinates matching X1(I)
- Y2(I) - ordinates matching X2(I)
- Y3(I) - ordinates matching X3(I)
- Y4(I) - ordinates matching X4(I)
- Z1(I,J) - values of Cp_{rp} for X1(I) and Y1(I)
- Z2(I,J) - values of Cp_{rp} for X2(I) and Y2(I)
- Z3(I,J) - values of Cp_{rp} for X3(I) and Y3(I)
- Z4(I,J) - values of Cp_{rp} for X4(I) and Y4(I)

Notation of Main Program VDR

A - variables in library routine IXCLOK used to evaluate computation times

ALF - values of α returned to VDR from INTSCS

ALFA - α input when experiment simulation is carried out

ALFC - α_{rpIII}

ALFCN - new value of α_{rpIII} for next iteration

ALFD - α_{rpIV}

ALFDN - new value of α_{rpIV} for next iteration

ALF1 - α_I

ALF2 - α_{II}

ALF3 - α_I

ALF4 - α_{III}

AM - mach number

CPA - $C_{p_{rpI}}$

CPB - $C_{p_{rpII}}$

CPC - $C_{p_{rpIII}}$

CPD - $C_{p_{rpIV}}$

EPSPS - relative difference between present static pressure and its value in the previous iteration

EPSPSG - convergence criterion (on the static pressure)

FALF - final α value (at convergence)

FPHI - final ϕ value (at convergence)

IA50 - a flag in IXCLOK

IA60 - a flag in IXCLOK

ICOPS - number of PS corrections carried out to ensure the C_p 's are in calibration range

IEPS - a flag governing the convergence criterion returned from INTSCS

IEPS1 - a flag governing the convergence criterion for probes I and II
 IEPS2 - a flag governing the convergence criterion for probes I and III
 IIT - number of iterations on p_s
 ISCAN - number of static pressure scans from initial static pressure guess upwards
 IXCLOK - system subroutine for computation time evaluation
 NOCOPS - a flag which when equal to 1 causes static pressure corrections to be carried out such that C_p 's are always inside calibration range, and when equal to 2 cause these corrections to be skipped
 NOSIM - a flag which when equal to 1 causes the program to simulate velocity measurement experiments and when equal to 2 causes the program to reduce measured data
 NX - number of calibration surface matrix abscissa's, α values (must be identical for all calibration surface matrices used)
 NY - number of calibration surface matrix ordinates, ϕ values (must be identical for all calibration surface matrices used)
 PDYN - dynamic pressure
 PHI - value of ϕ returned to VDR from INTSCS
 PHIB - ϕ_{rpII}
 PHII - ϕ input when experiment simulation is carried out
 PHI1 - ϕ_{rpI}
 PHI2 - ϕ_{rpII}
 PHI3 - ϕ_{rpI}
 PHI4 - ϕ_{rpIII}
 PPA - signal of probe in position I
 PPB - signal of probe in position II

PPC - signal of probe in position III
 PPC - signal of probe in position IV
 PS - static pressure
 PSIN - initial guess of static pressure
 PSN - new value of static pressure for next iteration
 PSC - corrected static pressure
 PST - memorized corrected static pressure
 PT - total pressure measured
 RELXPS - relaxation factor for convergence on the static pressure
 VIRTIM - virtual computation time
 XA - abscissas of calibration surface matrix of probe A
 XAX - transformed abscissas of calibration surface matrix of probe A
 XB - abscissas of calibration surface matrix of probe B
 XBX - transformed abscissas of calibration surface matrix of probe B
 XPC - yaw setting of position III
 XPD - yaw setting of position IV
 XRIN - α value at which scanning starts
 XRLU - lowest α value of calibration surface (as a condition it must be identical for probes A and B)
 XRUP - highest α value of calibration surface (as a condition it must be identical for probes A and B)
 YA - ordinates of calibration surface matrix of probe A
 YAX - transformed ordinates of calibration surface matrix of probe A
 YB - ordinates of calibration surface matrix of probe B
 YBX - transformed ordinates of calibration surface matrix of probe B

YPA	- pitch setting of probe A
YPB	- pitch setting of probe B
YRIN	- ϕ value at which scanning starts
YRLO	- lowest ϕ value of calibration surface (as a condition it must be identical for probes A and B)
YRUP	- highest ϕ value of calibration surface (as a condition it must be identical for probes A and B)
ZA	- Cp_{rpA} values of probe A
ZAX	- transformed Cp_{rpA} values of probe A
ZAMAX	- maximum of ZA array
ZAMIN	- minimum of ZA array
ZB	- Cp_{rpB} values of probe B
ZBX	- transformed Cp_{rpB} values of probe B
ZBMAX	- maximum of ZB array
ZBMIN	- minimum of ZB array

Introduction

Experimental knowledge of the flow field generated by rotating turbo impellers is of prime importance in the research and development of turbomachinery. It is essential for the refinement of design methods, for the development of new flow models which include secondary flow and tip clearance effects, and particularly for the verification of new computer codes developed to calculate the flow through rotating blade rows.

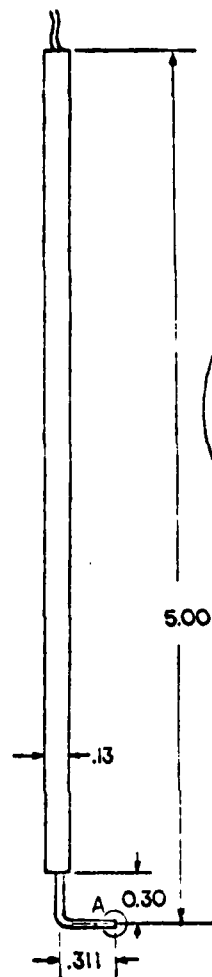
In recent years laser velocimeter techniques have been applied successfully to measure the flow both inside and downstream of rotors. (Ref. 1 for example). It has become clear however, that the laser techniques are only reliable in the hands of experienced investigators. A window which remains clean is essential, and seeding is usually required. Laser techniques do not measure the pressure field and usually can only measure two components of the velocity unless the axis of the laser is tilted. Difficulty is also encountered when measuring close to walls. Hence there are reasons to consider alternative techniques, particularly if they are simpler to apply routinely in stationary turbomachinery passages. Furthermore, the achievement of redundancy in measuring the flow field behind the impeller is itself a worthwhile goal. The present

work deals with the application of a particular system of small high response pressures probes at the exit of an impeller.

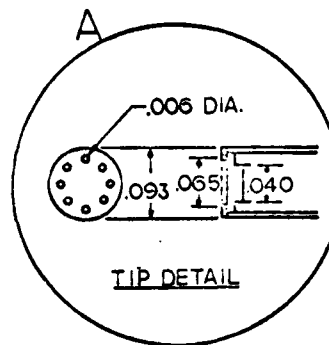
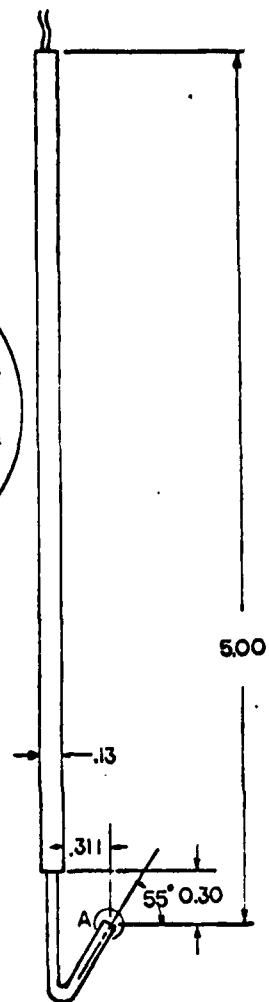
Measurements behind an impeller, in the stationary bladeless gap, are simpler to make than measurements within the rotating passages. Transducer probes can be installed through the stationary machine casing and the data transmitted without resort to slip rings or rotary transformers. The sensor is not subjected to the centrifugal field or to the vibration of the rotor. However, the flow to be measured is then fluctuating at blade-passing frequency and any system of sensors must be calibrated for a wide range of possible Mach number, pitch angle, yaw angle and pressure variation - and yet must be capable of the necessary frequency response.

In Ref. 2, a method was described for using two semiconductor pressure probes together with the technique of synchronized sampling, to obtain the distribution of the velocity vector downstream of a rotor. The geometries of the two probes, designated Type A and Type B, and their installation in the compressor annulus are shown in Fig 1. It was argued that, in principle, by rotating the probes in yaw about their tips and controlling the sampling of the data from each probe to be at the same position in the rotor frame, the system of two separate probes could be used to acquire data at a point in the periodic flow

TYPE A PROBE



TYPE B PROBE



TIP DETAIL

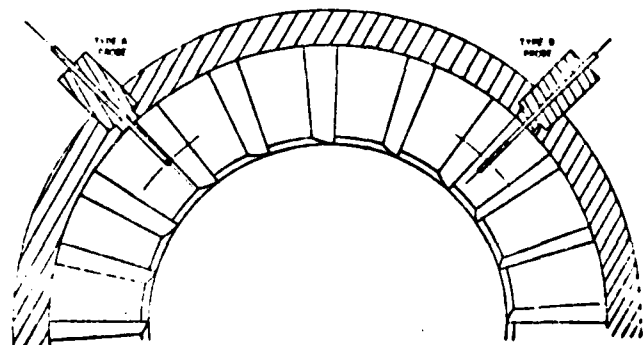
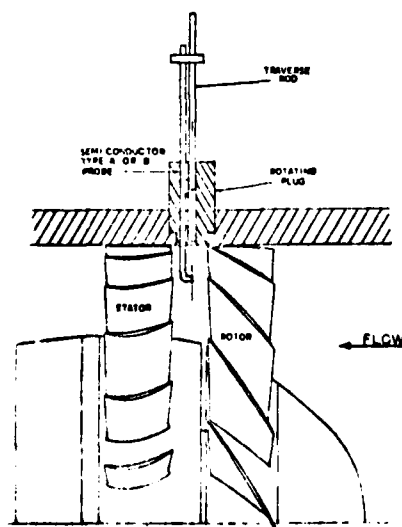


FIGURE 1. TYPE A AND TYPE B PROBES AND COMPRESSOR INSTALLATION.

from the rotor, corresponding to data normally obtained from the multiple sensors of four- or five hole pneumatic probes when measuring velocity in steady flows. The technique promised the use of probes having the simplest geometry and thus avoided the large size, expense and unreliability of multiple sensor probes which incorporate multiple semi-conductor transducers (Ref. 3). Because of the simple sensor tip geometry (that of a cylinder at incidence to the flow) the unsteady response was likely to be as good as could be expected of any single physical sensor.

The two-probe technique is strictly applicable only to periodic flows. However, data obtained on successive rotations of the rotor can be averaged to eliminate fluctuations which are not periodic. This was shown to be effective in tests reported in Ref. 2 in which a single Type A probe was used to establish the peripheral blade-to-blade distribution of flow yaw angle.

In order to obtain velocity from the pressure measurements which can be obtained from the two probes, the steady response characteristics must first be established in calibration tests carried out in a known, controlled, uniform flow. Second, a method of applying the calibration to measurements made in an unknown flow must be devised. In the present method two different approaches have been followed. In Ref. 4, a technique is given for representing

and applying the probe calibration analytically. When first applied the method gave surprisingly good accuracy (1 - 2%) since the method required that the probes had characteristics which could be well represented analytically. This in turn required that the probe tips be geometrically precise, a feature which was not present in the first generation of probes.

A second, more general approach is reported here, wherein the calibration of each probe is represented by a two-dimensional array of pressure coefficients. The application of the calibration given in this form, in an unknown flow required the development of special numerical procedures. The purpose of the present report is to document the analysis and the Fortran program developed to apply the method.

In its present form, the method does not require that the calibration "Surfaces" be symmetrical about any axis or be expressed in analytical form, but does require that the pressure coefficient be independent of Mach number. The latter restriction could undoubtedly be removed by introducing additional iterative steps. Further, in the present method only five measurements have to be taken to determine uniquely a velocity vector at a point. Throughout the report, the Fortran program notation has been used to describe the physics and equations involved in the solution.

Mathematical model

Assume the A and B type probes of ref. [1] (see also fig. 1) to be immersed in a three-dimensional steady flow field.* The pressure response of each of these probes in given gas is functionally described by four variables as:

$$P_p = P_p(\alpha, \phi, P_T, P_S) \quad (1)$$

If a pressure coefficient is defined as

$$C_{p_{rp}} = \frac{P_p - P_S}{P_T - P_S} \quad (2)$$

The calibration surface of each probe is given in the general case in form of a matrix of values of C_p , where

$$C_{p_{rp}} = C_{p_{rp}}(\alpha_{rp}, \phi_{rp}) \quad (3)$$

The pressure coefficient defined in this way has only a second order dependence on Mach and Reynolds numbers in the range of

* For our purpose, using the synchronized sampling, the flow field behind the impeller is steady, although the probes require a high speed response because of fluctuations.

$0 < Ma < 0.7$ in turbulent flows (Ref. 2), so that, to first order their influence is neglected in writing eq. (3).

If the type A probe is rotated about its axis into three different positions ($i = I, III, IV$) readings are taken, and the type B probe is fixed in position II and a single reading is taken, the following four equations can be written.

$$\begin{aligned} C_{p_{Ai}} &= \frac{P_{p_{Ai}} - P_S}{P_T - P_S} = C_{p_{Ai}}(\alpha, \phi) \\ C_{p_{BII}} &= \frac{P_{p_{BII}} - P_S}{P_T - P_S} = C_{p_{BII}}(\alpha, \phi) \end{aligned} \quad (4)$$

it should be pointed out here, to avoid misunderstanding that α and ϕ are defined in a coordinate system relative to the machine axis and not relative to the probe axis. In the set of four equations (4) there are four unknown quantities, namely: α , ϕ , P_T and P_S . These are the quantities to be evaluated using the measured data. Together with the stagnation temperature they define the flow field uniquely. The four equations, resulting from the four measurements, should be sufficient to determine the four unknown quantities.

But the problem is complicated by three facts:

- 1) The calibration surfaces are not generally known in analytical form.
- 2) The calibration surfaces are double valued in α and ϕ i.e., for a given C_p and α there exist two ϕ values, or for a given C_p and ϕ there are two α values which satisfy eq. 3.

- 3) As a result of the measurement the value of P_p rather than of C_p is determined.

Since the calibration surfaces are not given in a simple analytical form the solution has to be numerical. An iterative procedure is required because P_p and not C_p values are measured. First P_s and P_T have to be guessed to yield C_p values, knowing the four measured values of P_p , and using eq. 4. The guess is then iteratively corrected to converge on the solution. However, convergence of the iterative procedure is complicated because of the double valued nature of the calibration surfaces.

This method of iteration shown in Fig. 2 was attempted initially for the evaluation of a measured point. In practice the initially suggested procedure converged in some cases and diverged in others, depending on the values, and signs of α and ϕ . This was not surprising as convergence on two variables is not likely to be a simple matter. However, in order that the measurement technique be useful, convergence on the correct solution for a general set of measurements, is absolutely necessary. In practice, this can certainly be achieved if one of the two iteration variables is obtained by measurement. Since the static pressure is a difficult quantity to measure even in a steady flow field, only the stagnation pressure measurement need be considered. It is possible that the time-varying stagnation pressure could be measured with a suitably designed Kiel probe. Data would then be taken by synchronized sampling from the fixed Kiel probe, from the type A probe rotated into two positions, and from the

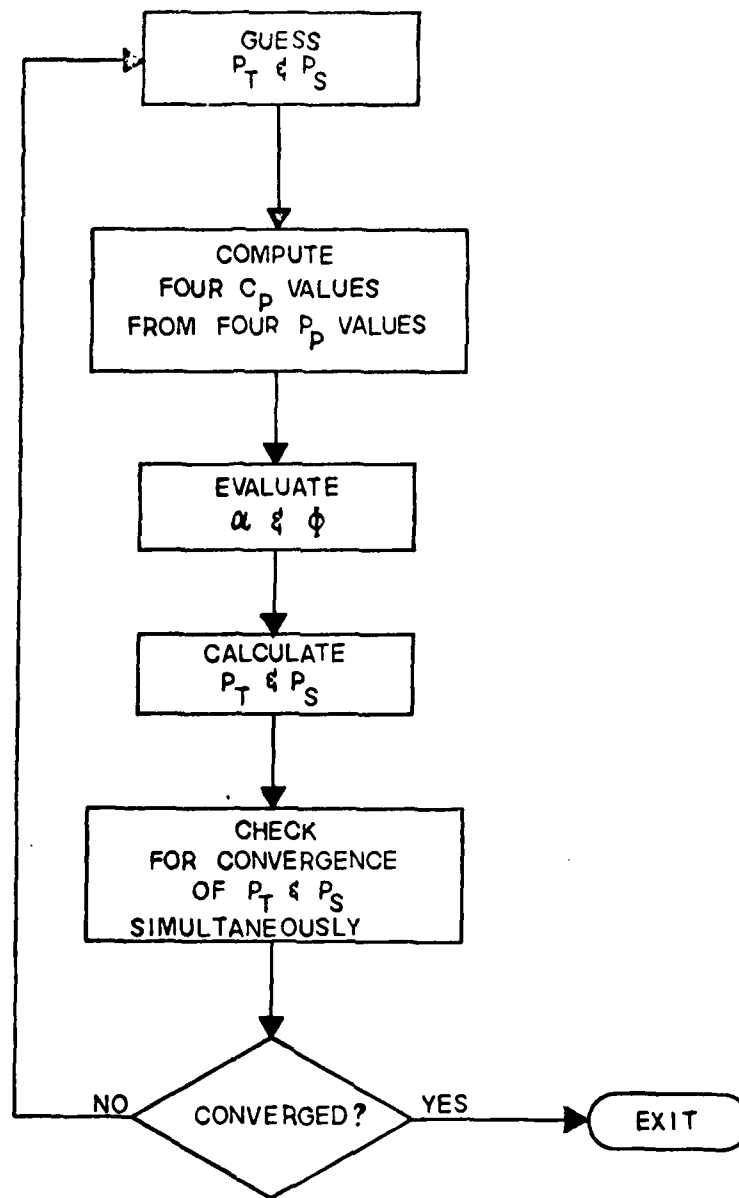


Fig. 2: Unstable iterative solution using measurement of A type and B type probes only.

fixed type B probe. The method of solution is then as shown in Fig. 3. The method shown in Fig. 3 proved to converge under all conditions. It is described in detail in the following pages.

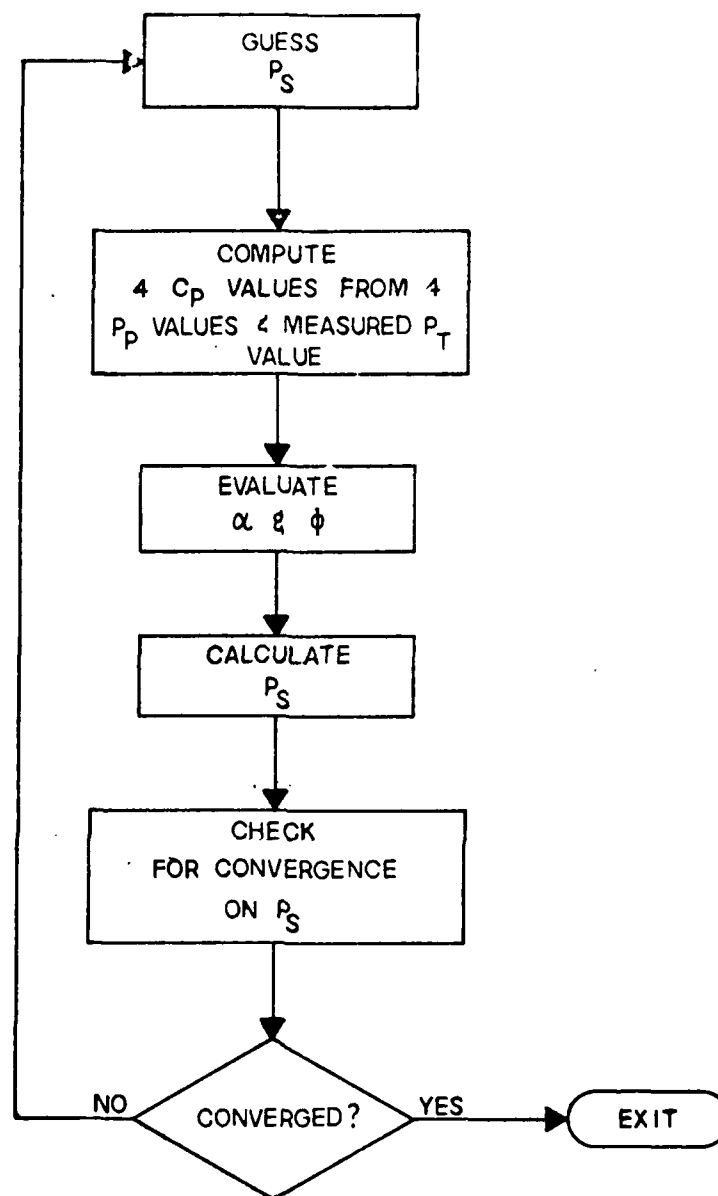


Fig. 3: Stable iterative solution using measurements of A type and B type probes as well as measurements of a Kiel probe.

Evaluation of α and ϕ (method)

The best way to understand the evaluation of yaw and pitch is to look at it from a topographical point of view. Each of the type A and type B probes has a unique calibration surface $Cp_{rp} = Cp_{rp}(\alpha_{rp}, \phi_{rp})$, where α_{rp} and ϕ_{rp} are measured relative to the axis of symmetry through the sensor at the probe tip. The calibration surface in this representation is invariant to yaw and pitch of the probe axis relative to the laboratory space. The same calibration surface if represented in the form $Cp = Cp(\alpha, \phi)$ can be written as

$$Cp = Cp[(\alpha_p + \alpha_{rp}), (\phi_p + \phi_{rp})] \quad (5)$$

where α_p and ϕ_p are the probe tip axis angular settings relative to the laboratory space. It is clear from eq. (5) that Cp can be derived from Cp_{rp} by a constant translation: α_p, ϕ_p on the α, ϕ plane. As each Cp_{rp} can be viewed as a hill with its peak at $\alpha_{rp} = 0$ and $\phi_{rp} = 0$. The Cp surfaces are the same hills with their peaks translated to $\alpha = \alpha_p$ and $\phi = \phi_p$.

In the present method probe A is used in three different angular settings namely:

$$1) \quad \alpha_p = 0 \quad \phi_p = 0$$

$$\text{III) } \alpha_p = \alpha_{p\text{III}} \quad \phi_p = 0$$

$$\text{IV) } \alpha_p = \alpha_{p\text{IV}} \quad \phi_p = 0$$

and the B probe is used in a fixed position, namely:

$$\text{II) } \alpha_p = 0 \quad \phi_p = \phi_{p\text{II}}$$

For this case the topography of the calibration surfaces will appear as four hills. The three with their peaks at points $(0,0)$; $(+\alpha_{p\text{III}}, 0)$ and $(-\alpha_{p\text{IV}}, 0)$ are the translated hills $C_{p\text{rpA}}$ and the fourth with its peak at $(0, \phi_{p\text{II}})$ is the translated hill $C_{p\text{rpB}}$. Their contours of constant C_p are then as shown in figure 4.

Assume now that a velocity vector with yaw α and pitch ϕ is to be measured. These values of α and ϕ will be sensed uniquely by the probes at their four angular settings. Were equation (4) single valued, the values of α and ϕ could be uniquely evaluated, as the single intersection point between the projections of appropriate lines of constant C_p on the α, ϕ plane*. In the present case of the double valued functions, the lines of constant C_p are closed curves and more than a single intersection point do exist.

* C_p has generally a different value for each probe in each of its settings. Thus the solution involves solving for the intersection points between projections of contours of specified (but different) C_p values on the different hills.

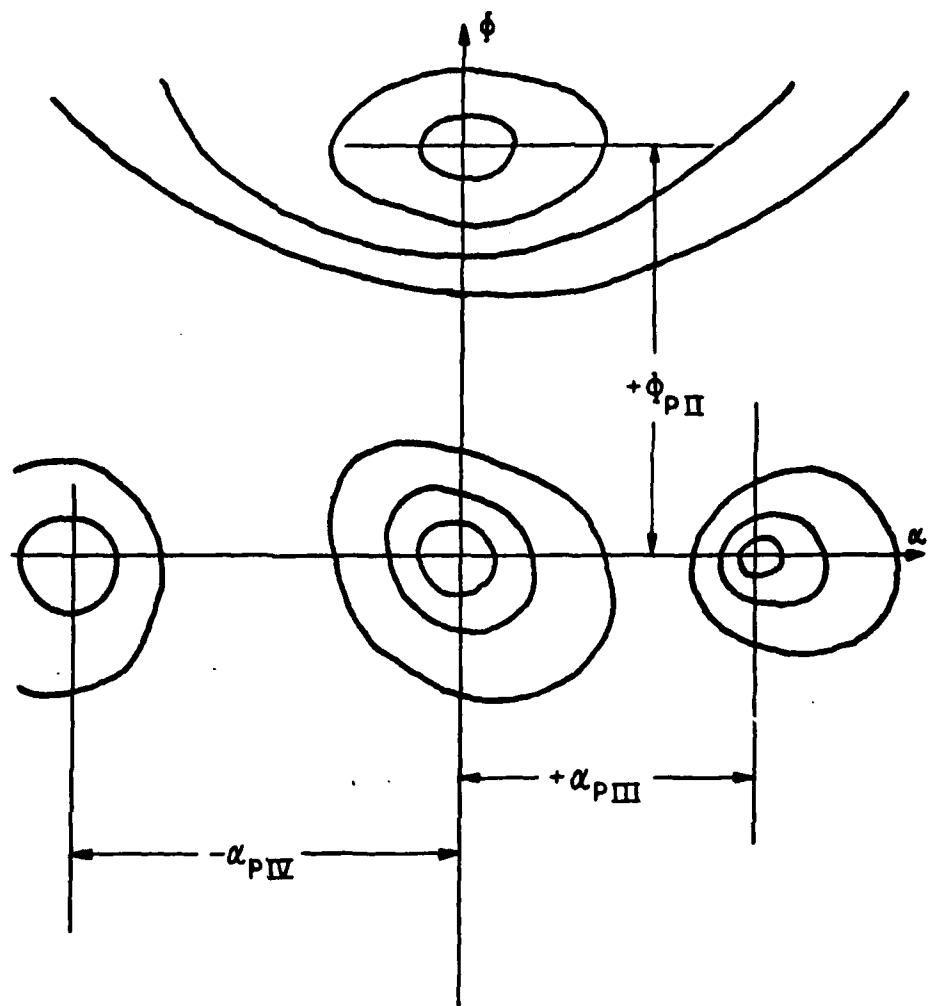


Fig. 4: Projections of $C_p = \text{const.}$ lines of the four calibration surfaces (the center hill is for probe A at $\alpha_p = 0$, $\phi_p = 0$, the top hill is for probe B at $\alpha_p = 0$, $\phi_p = \phi_{pII}$, the right hill is for probe A at $\alpha_p = +\alpha_{pIII}$, $\phi_p = 0$ and the left hill is for probe A at $\alpha_p = -\alpha_{pIV}$, $\phi_p = 0$).

The situation is shown in Fig. 5 for an example of a number of such intersection points. The correct intersection point, however, is uniquely identified as the only point through which all four $C_p = \text{const.}$ curves pass.

From an examination of Fig. 5 it is clear that the intersection points of three closed C_p curves projections only are sufficient to identify α and ϕ uniquely. However one of these three curves must be that belonging to the type B probe.

The details of the numerical procedure used to obtain the correct intersection point in the evaluation of α and ϕ , are given in the following paragraph.

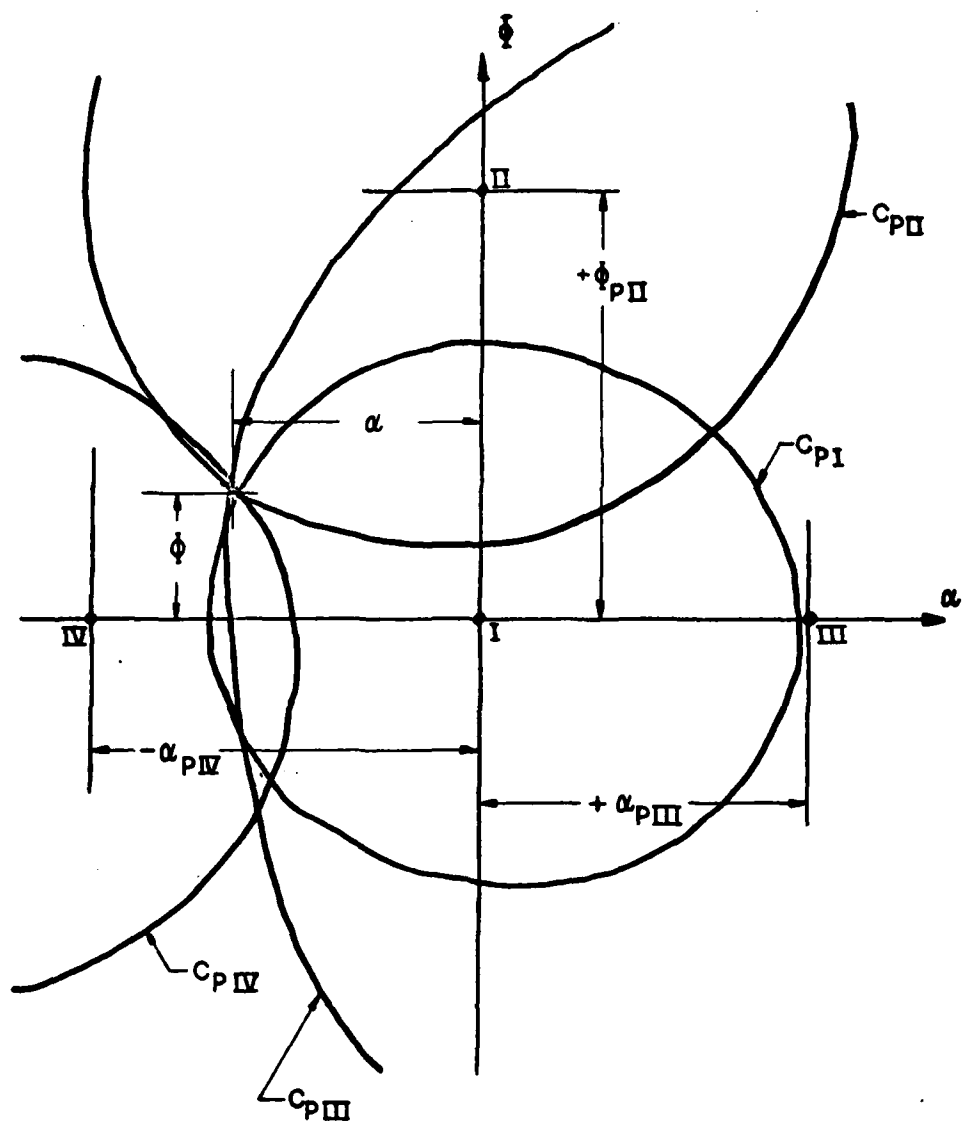


Fig. 5: An example showing a number of intersection points. The real one is in the second quadrant.

Evaluation of the intersection point coordinates (numerical Procedure)

The calibration surfaces Cp_{rp} are represented in form of a linear string of values ordered into an array, as shown schematically in figure 6. The numbers in Fig. 6 indicate the position of a Cp_{rp} value in the string. The string starts with the value of Cp_{rp} at a point $(-\alpha_{rpLo}; -\phi_{rpLo})$ and ends with the value of Cp_{rp} at a point $(+\alpha_{rpUp}; +\phi_{rpUp})$. This sequence must be kept and can not be changed.

Each of the closed $Cp = \text{const.}$ curves projections in figs. 2 and 3 is the projection of the line of intersection between a plane parallel to the α, ϕ plane at a height equal to Cp and the calibration surface. These closed curves can be determined as the locus of the projections of all the penetration points of arbitrary lines parallel to the α, ϕ plane at a height Cp and the calibration surface. Such penetration points are calculated in subroutine "PENPTS", Fig. 10.

PENPTS calculates the first two penetration points of a surface Z (in the present case $Z = Cp$) by a straight line piercing that surface. If the surface is double valued these two points are the only roots. The surface is given as a table of numbers on a cartesian basis $Z = Z(X, Y)$ (or in the present case $Cp = Cp(\alpha, \phi)$).

The subroutine has the following limitations:

- 1) No roots can be found on the lower $Y = \text{const.}$ boundary

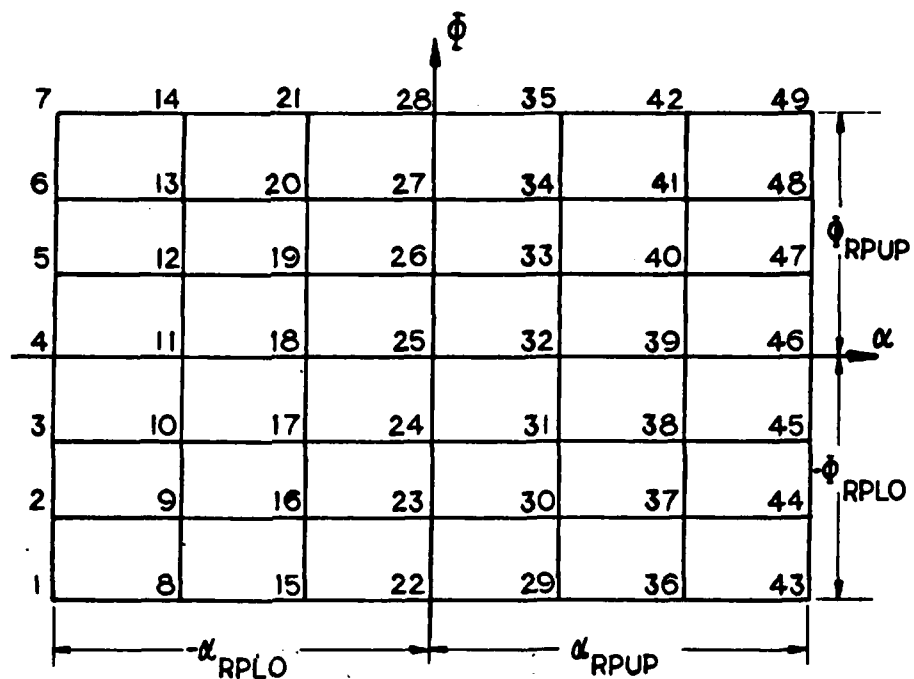


Fig. 6: The order of a calibration surface array.

- 2) The roots can be found only along a piercing line which is parallel to the X axis (but at any height above the X,Y plane)
- 3) The table $Z = Z(X,Y)$ defining the surface must be based on a grid comprising lines $X = \text{const.}$ and $Y = \text{const.}$ The spacing of these lines must not be equal. In other words the surface is defined by a rectangular grid in the X,Y plane, from X_{\min} to X_{\max} and from Y_{\min} to Y_{\max} .
- 4) Only a single root can be evaluated in a surface element located above a defining rectangle on the X,Y plane.
- 5) Not more than the first two roots will be evaluated for any piercing line.
- 6) The surface must be monotonic over each rectangle (this is a result of limitation 4).
- 7) All X and Y arguments must be given in increasing order.

These limitations do not restrict the application of PENPTS in the present problem as long as the calibration surfaces are smooth within the element located above a grid rectangle. However, the elemental grid rectangles can be reduced arbitrarily in size. If a calibration surface is more than double valued PENPTS will fail. However in this case the probe yielding such a calibration surface can not be considered a useful instrument unless used only in parts of the domain where it is double valued.

Z is defined from X_{\min} to X_{\max} and from Y_{\min} to Y_{\max} . PENPTS is given the following initial information: X values and Y values defining grid points, corresponding Z values, the Y location (YG) and the height above the X,Y plane (HT) of the piercing line. With this information PENPTS searches for the band of rectangles which includes YG or of which YG is the lower boundary (see fig. 7) and then scans this band from left to right in search for penetration points. The scanning is based on the geometry given in fig. 7 which represents a particular element in the band, approximated by two plane triangles.

Initially a coarse scan is carried out just to detect, but not to evaluate, an intersection point. This is done checking for each sub-domain whether $(ZX(I-1) - HT)/(ZX(I) - HT) \leq 0$. If this condition is true a root is detected and control is transferred to its exact evaluation. The value of the root is calculated after its location, either in the first (left) or second (right) triangle is determined (each grid rectangle is composed of two triangles). Equation 6 which is based on fig. 8 (for a left triangle) or eq. 7 which is based on fig. 9 (for a right triangle) is used to evaluate the penetration point. These equations express the linear interpolation of C_p in the Fortran rotation used in this program.

$$XS = X(I-1) + \frac{ABS(ZX(I-1)-HT)*(XM-X(I-1))}{(ABS(HT-ZM) + ABS(ZX(I-1)-HT))} \quad (6)$$

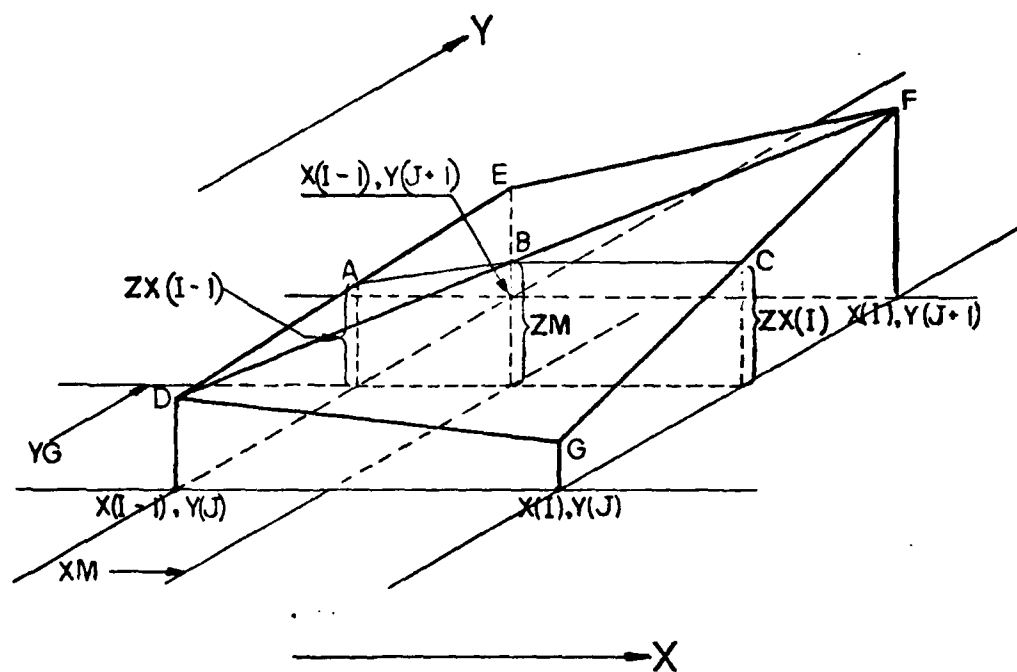


Fig. 7: The geometry of a linearized calibration surface element comprising two plane triangles and its intersection with a plane normal to X, Y along $Y = Y_G$.

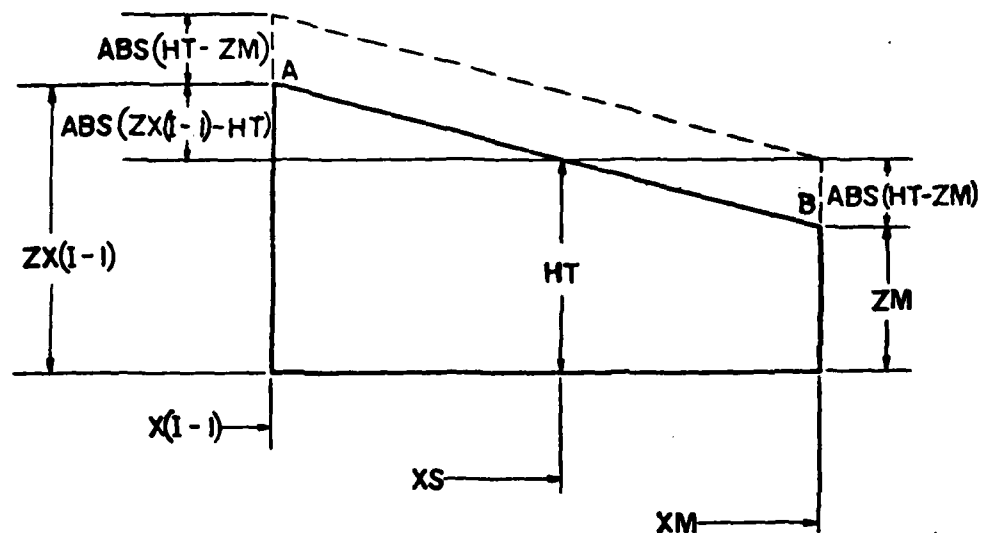


Fig. 8: The geometry for a penetration through a left hand (first) triangle.

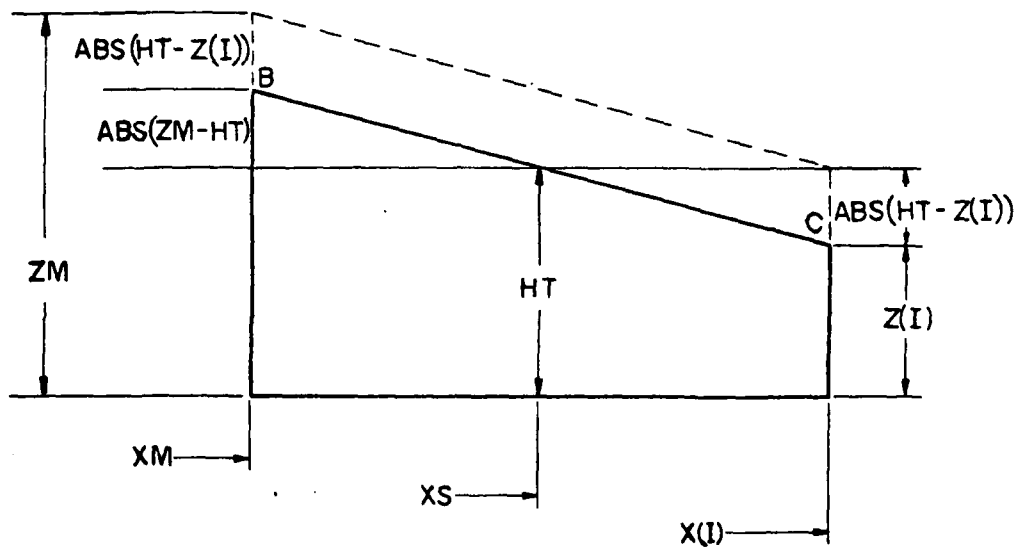


Fig. 9: The geometry for a penetration through a right hand (second) triangle.

$$XS = XM + (X(I)-XM)*ABS(ZM-HT)/(ABS(ZM-HT) + ABS(HT-Z(I))) \quad (7)$$

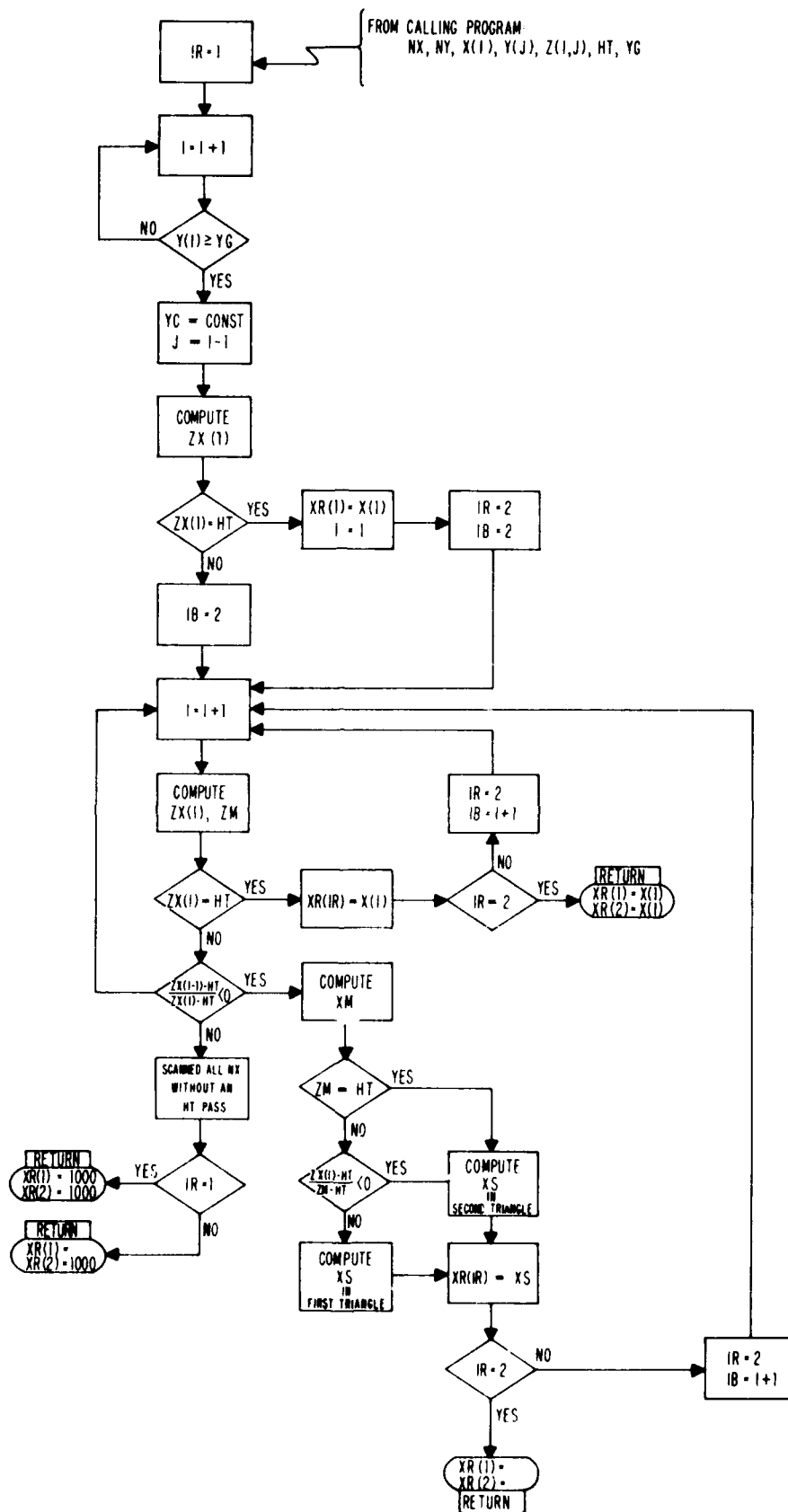
Equations 6 and 7 are invariant to the slope of the calibration surface i.e., the slope of the straight lines AB and BC.

Finally it should be pointed out that when two penetration points are determined the values of their abscissas, $X(I)$, are returned. When only a single penetration point is detected the abscissa $X(2)$ will be returned with a value of 1000.0. When no penetration point is determined both $X(I)$ values returned will have the value of 1000.0. The program logic is designed to recognize these messages.

It was stated earlier that PENPTS is used to determine the closed intersection curves projections on the X,Y plane. In fact not the curves but just the intersection points between each two of them are required (see figure 3).

To compute the coordinates of these points the subroutine "INTSCS" is used. It uses PENPTS as a subroutine.

In INTSCS a scanning procedure is carried out from a minimal value of Y (or ϕ) YRIN to an upper value of YRUP, or a



prescribed 10,000 times* which ever comes earlier. The subroutine scans through any two arbitrarily chosen closed curve projections to find their intersection points. In each scan (I) up to four penetration points can be determined, while the penetration points of the previous scan (J) are memorized. Together, eight penetration points can be involved. When no intersection point exists the geometrical situation is as shown in figure 11, while the existence of an intersection point is characterized in figure 12. Subroutine INTSCS can distinguish between the two situations. In figures 11 and 12 the case of four penetration points found in each scan are shown. The subroutine, however will handle any possible number of such points, from zero to four. A "no penetration points" is assigned an abscissa value of 1000.0 by PENPTS as explained earlier.

When an intersection point is detected its evaluation is based on the geometry shown in fig. 12. The eight penetration points have the following coordinates:

AJL(RAJL,YRJ)	BJL(RBJL,YRJ)
BJR(RBJR,YRJ)	AJR(RAJR,YRJ)
BIL(RBIL,YR)	AIL(RAIL,YR)
AIR(RAIR,YR)	BIR(RBIR,YR)

* The 10,000 scans are governed by a program constant in the line "DO 140" and can be arbitrarily varied.

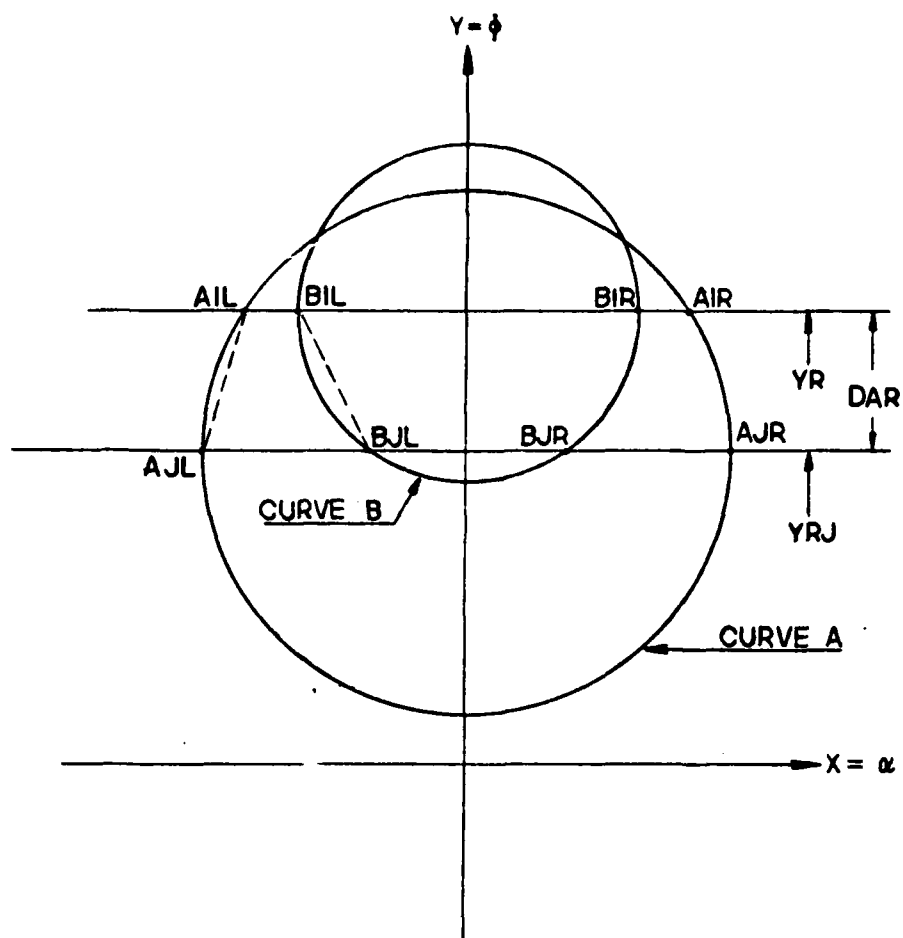


Fig. 11: The geometry for two successive scans when no intersection point exists.

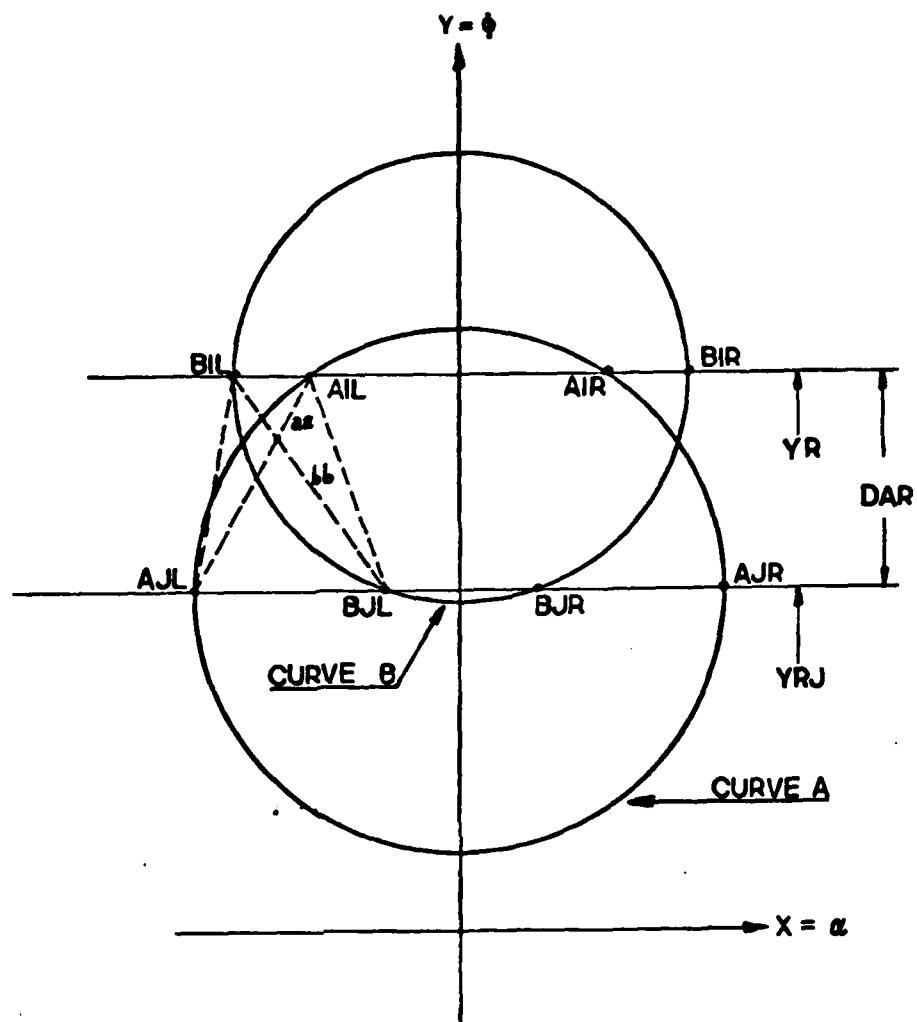


Fig. 12: The geometry for two successive scans when an intersection point does exist.

The left intersection point illustrated in fig. 12 is the intersection point of the lines aa and bb, each described by its equation:

$$\text{for aa } Y = (AA)X + BA \quad (8)$$

$$\text{for bb } Y = (AB)X + BB \quad (9)$$

The constants AA, BA, AB and BB are given in equations 10 to 13.

$$AA = (YRJ - YR) / (RAJL - RAIL) \quad (10)$$

$$BA = YR - AA * RAIL \quad (11)$$

$$AB = (YRJ - YR) / (RBJL - RBIL) \quad (12)$$

$$BB = YR - AB * RBIL \quad (13)$$

The coordinates of the intersection point to be calculated are

$$X = (BB - BA) / (AA - AB) \quad (14)$$

$$Y = X * AA + BA \quad (15)$$

These relations are true for a left hand intersection point. Analogous equations are true for a right hand intersection point. In this algorithm the straight lines aa and bb approximate the curved lines connecting AJL with AIL and BJL with BIL or similar lines on the right hand side of figure 12. The error introduced through this approximation is reduced as $DAR = \Delta\phi$ is reduced.

It is possible that an intersection point is identical with AIL and BIL or AIR and BIR. This case is defined as "direct hit". The program is designed to detect such a direct hit and evaluate the corresponding intersection point accordingly.

The above algorithm works perfectly as long as the two closed $C_p = \text{const.}$ curves are far from being tangent. But in

practice a situation of almost tangent curves can arise when X (or α) is very small. In this case the preceding algorithm will fail and must be replaced. The geometry of this situation is described in figure 13. This situation is identified by INTSCS and the intersection points are then evaluated assuming that they are intersections of two circular arcs. When the curves $C_p = \text{const.}$ are almost circular this approximation does not lead to unacceptable errors.

It was stated earlier that INTSCS scans from a minimum value of ϕ to a maximum value of ϕ with prescribed steps $\Delta\phi$, as shown in figs. 11 and 12. This direction of the scanning is used when the intersection points of the curves C_{p_I} and $C_{p_{II}}$ of fig. 5 are evaluated.

However, in course of the reduction of the measured data, scans in the direction of α in steps of $\Delta\alpha$ are also necessary to evaluate the intersections of the curves C_{p_I} and $C_{p_{III}}$ or C_{p_I} and $C_{p_{IV}}$. INTSCS is designed to carry out this task as well. To do this the calling statement for INTSCS is appropriately changed as will be explained in the next section. To be general enough INTSCS is not written in terms of α and ϕ or X and Y but rather in terms of general arguments. The best way to understand INTSCS is to compare its general arguments to physical quantities by means of the calling statements. In fig. 14 the flow diagram in INTSCS is given in terms of the general arguments.

INTSCS returns to the main program (fig. 15) the (α, ϕ) coordinates of two intersection points between the $C_p = \text{const.}$ curves specified in the calling statement. Let us now follow the way in which the main program is designed to utilize INTSCS

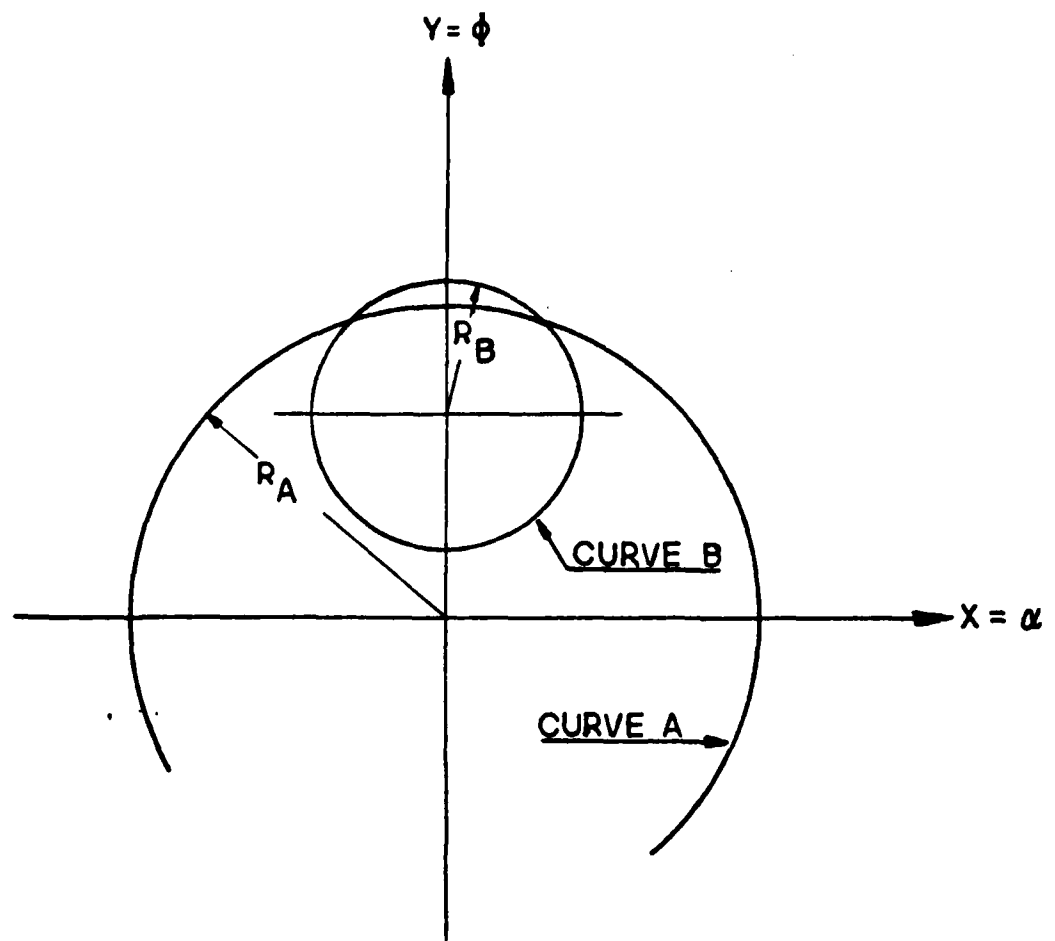


Fig. 13: The geometry when two closed $C_p = \text{const.}$ curves are almost tangent.

for the evaluation of α and ϕ of the velocity vector, as well as static and total pressures.

Evaluation of the Velocity Vector and Pressures from the Probe Signals

Fortran program VDR was written to evaluate the velocity vector from probe measurements of pressures. The program is shown in Fig. 15.

At line 1410 INTSCS is called to scan curves I and II for possible intersection points. Scanning can be carried out in the direction of the ordinate only, with the calibration curve matrices compiled exactly as shown in fig. 6. This limitation is imposed by the way PENPTS is constructed. In the case of the intersection points between I and II ZA and ZB are scanned without difficulties in the direction of the ordinate which is ϕ as shown in fig. 12 and returns with the coordinates of the two first intersection points, points 1 and 2 of Fig. 16. They are ALF1, PHI1 and ALF2, PHI2. In line 1500 INTSCS is called again to scan curves I and III. Now scanning has to be carried out in the direction of the abscissa, a task for which INTSCS was not designed. To overcome this problem the calibration curve matrices are used in a transformed form such that the previous abscissas are now ordinates, ordinates are abscissas and the internal structures of the Cp_{rp} arrays are accordingly modified. This transformation is carried in VDR in the section between lines 320 and 450. Comparison of the calling line 1500 to the previous calling line 1410 shows very clearly how the various arrays: original and transformed, are used. The coordinates of points 3 and 4 of fig. 16

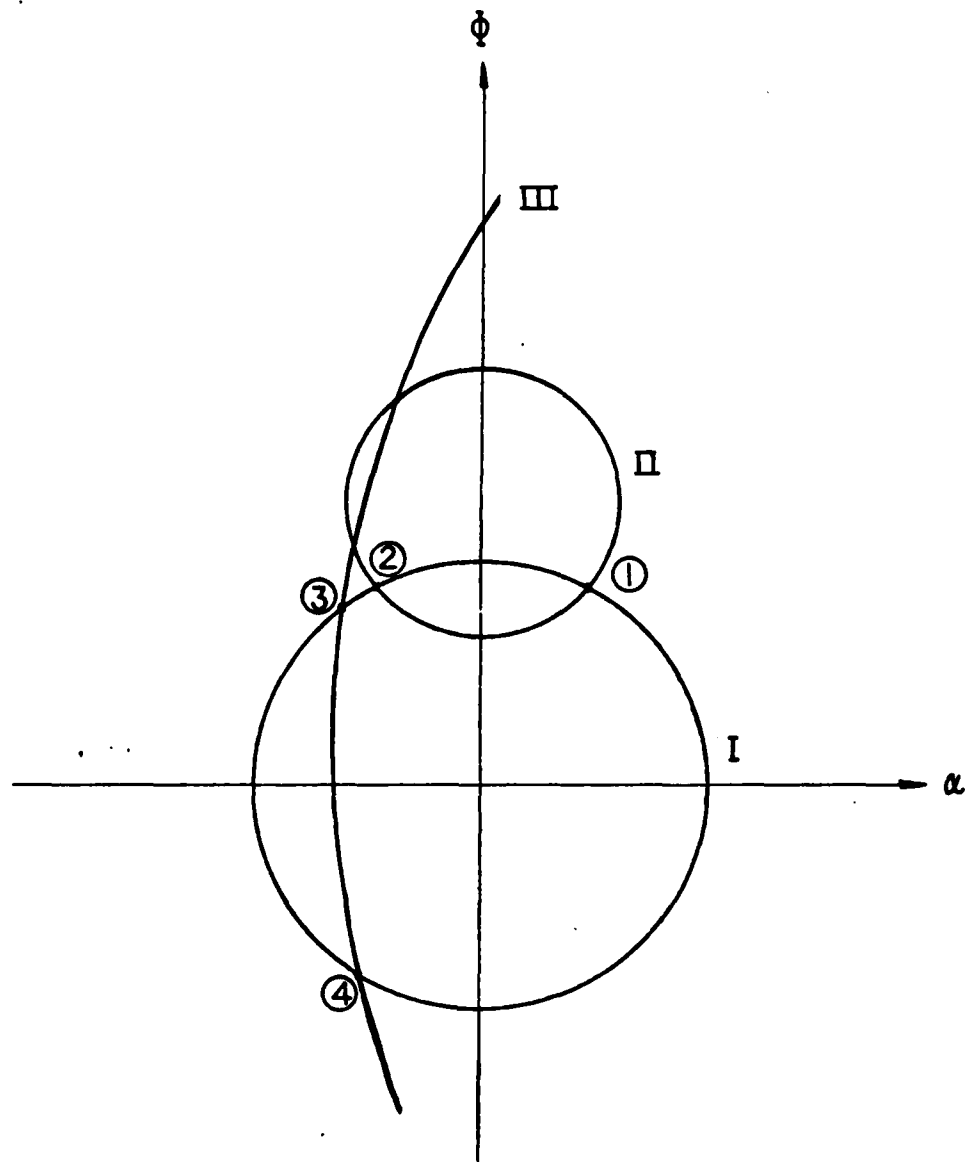


Fig. 16: Selection of the proper intersection point in VDR.

are now returned to the main program of VDR, they are ALF3,PHI3 and ALF4,PHI4.

We are seeking a single intersection point; the one representing yaw and pitch as sensed by probe A in positions I and III and probe B in position II. But, as the calibration surfaces are double valued we are now, unfortunately, in the possession of four points. The solution, however, is physically unique. Only a single velocity vector exists in reality and its yaw and pitch are included in the four intersection points evaluated. Were both the measurements and the numerical procedure absolutely accurate, two of the four points would have been identical. But this is not the case in reality, instead of a single point, two points close to each other will be detected. Therefore the average coordinates of the two of the four intersection points returned to VDR from INTSCS which are closest to each other are selected as the measured yaw and pitch angles. In the example shown in fig. 16 this will be the point dividing the distance between points 2 and 3.

The calculation is now at the point at which α and ϕ are temporarily known (see fig. 3). Using α and ϕ a new $C_{p_{rpIV}}$ (for probe A in position IV) is computed by linear interpolation using subroutine INTPLT. With this new value of $C_{p_{rpIV}}$ and with P_{pIV} a new P_s is computed. If this new value of P_s is close enough as determined by EPSPSG to the guessed value, or to the value of P_s in the previous iteration, the data reduction for the particular point in question is terminated.

The relative difference between present and previous P_s is compared to the convergence criterion EPSPSG. This criterion is evaluated by an empirical function determined to give best compromise between accuracy of results and computer time required until convergence is achieved. When the calculation follows normal routine the convergence criterion is given in line 1710 as function of P_T . When the routine for almost tangent curves is used during data reduction either on the right or the left side a different empirical function (lines 1720 or 1730) is used.

If the convergence criterion is satisfied results are printed out and data for a new measurement point is read for reduction. If, however convergence is not reached a new static pressure for a next iteration is evaluated (line 1780).

Convergence and accuracy

The convergence of the present iterative procedure is not ensured in all possible cases of data sets. The program, however, is adjusted to converge in most of the cases. Similarly to other iterative computation method some experience is required to achieve convergence when the calculation does not converge. In this paragraph the principal factors affecting convergence, computation time and accuracy, which are obviously coupled, are pointed out.

The convergence and accuracy of reduction of a data set: P_T , PPA, PPB, PPC, PPD, PSIN (or analogous set in the experiment simulation mode) depends on the following factors, which can be varied by the user.

- 1) Coarseness of calibration arrays ZA, ZB and their linearity. With coarser arrays convergence problem will increase and accuracy of results decrease.
- 2) Probe settings YPB, XPC, XPD (with the following probe settings being fixed and not variable $YPA = YPC = YPD = 0.0$; $XPA = XPB = 0.0$). The optimum setting is about $+20^\circ$ to 25° . Too small values reduce accuracy, too big values cause convergence problems and probe tip flow separation.
- 3) RELXPS, the static pressure relaxation factor. The smaller this factor the safer will convergence be achieved. Computation time, however, will increase.
- 4) The constant 5.0 in line 1050 of the program. The dimension of this constant is kg/m^2 . If too big results can be lost and if too small computer time will be growing. The variation of this constant should be coupled with an appropriate modification of the constant in line 1010 of VDR (item 8 in this list).

- 5) The constants in the evaluation of EPSPSG (lines 1710 to 1730). The smaller EPSPSG the more accurate the results in expense of increased computation time and reduced convergence safety.
- 6) The constant scanning step DAR. The smaller DAR the more accurate the results, but too small values can cause complete loss of results. Computation time increases with reduced DAR.
- 7) The constant 10 in line 1360. This constant governs the number of P_s corrections.
- 8) The constant 1000 in line 1010. This constant governs the number of scans.

If convergence is not achieved in a particular case variation of each or of a combination of the above values will always enable convergence.

Evaluation of the Computation Time

By deleting the letters CT from column 1 and 2 of lines 20 to 70, 1930 to 1960, 1980, 2000, 2010 the actual computation time as well as CPU time are evaluated and printed out. The following statement prior to execution is required in this case:*

GLOBAL T SYSLIB SSPLIB

This option is useful for adjusting the constants affecting convergence as to optimal compromise between accuracy, ease of convergence and calculation costs.

* When the program is run on Naval Postgraduate School IBM 360 system.

Input

- 1) Calibration arrays have to be input in the following manner: first values of NX and NNY , second values of X in rising order, third values of Y in rising order and fourth values of Z in the order shown in Fig. 6. Two calibration arrays are read: first the array of type A probe and second the array of type B probe.
- 2) If the program is run in experiment simulation mode PT and PS are read in Kg/m^2 and subsequently ϕ and ϕ .
- 3) If the program is run in data reduction mode the measured values of PT , PPA , PPB , PPC and PPD are read and then the guess of static pressure $PSIN$. All are read in Kg/m^2 . $PSIN$ has to be lower than the actually existing value to ensure convergence of the calculation. Too low a value will cause waste of computer time.

Calibration arrays are read from a disk space on which they are stored. The following statement prior to execution is required for successful reading:

```
FILEDEF 02 DSK NAME XX
```

here NAME is the name of the file on which the calibration data of probes A and B is stored in proper order and format, XX is a two digit number.

Simulation or measurements reduction input is read in the normal way using the terminal keyboard or punched cards.

Output

α , ϕ , P_S , P_T and Ma are printed out according to lines 1820 to 1920. This output, however is not sufficient when the logic of the computation is to be followed either to examine the execution of the program or for debugging. Two programs with additional output are given in appendices 2 and 3 and can be used for this purpose. The first, SWVDR gives short additional output, namely:

- 1) When PSIN is successively increased automatically by the program to ensure convergence, the values of PSIN are printed out.
- 2) IIT, FALF, FPHI and PSN are printed out at the end of each iteration prior to the convergence test.

The second program WVDR prints more detailed information. All additional WRITE statements in this program are numbered with three digit numbers starting with 9.

Conclusions

The following conclusions are drawn on the basis of experience gained in running the program with various data sets and various types of calibration surfaces.

- 1) Optimal probe settings for ease of convergence and high accuracy are: $YPB = 250$, $XPC = 250$, $XPB = -250$. It is therefore suggested that a B type probe with 250 pitch will be used, and that the A type probe be rotated to ± 250 .
- 2) Convergence and accuracy, as well as computer time efficiency are improved when the calibration surfaces of both probes are not flat at their peaks but are rather rounded. It is therefore suggested that a new probe tip geometry be considered. A spherical tip with a central pressure tap is recommended. To prevent damage to the sensitive transducer located behind the pressure tap, and in order to improve the frequency response of the probes it is suggested that the volume between the pressure tap face and the transducer be filled with an appropriate liquid that will not affect the transducer negatively. In this case the opening of the pressure tap has to be sealed with a very thin low inertia membrane.
- 3) It is probably possible to modify the iterative procedure such that safe convergence can be achieved also when using the scheme of Fig. 2. If this can be achieved the Kiel probe will not be necessary. An effort in this direction is suggested.

References

1. Dunker R. J., Strinning P. E., and Weyer, H. B., "Experimental Study of the Flow Field Within a Transonic Axial Compressor Rotor by Laser Velocimetry and Comparison With Through-Flow Calculations", ASME Journal of Engineering for Power, Vol. 100, pp. 279-286, April 1978.
2. Shreeve, P. P., Simmons J. M., Winters K. A., and West J. C. Jr., "Determination of Transonic Compressor Flow Field by Synchronized Sampling of Stationary Fast Response Transducers", Symposium on Non-Steady Fluid Dynamics, ASME 1978 Winter Annual Meeting, San Francisco, Dec 1978. (To be published in ASME Journal of Fluids Engineering)
3. Thompkins W. T. Jr., and Kerrebrock J. L., "Exit Flow From a Transonic Compressor Rotor", AGARD Conference Proceedings No. 177, Unsteady Phenomena in Turbomachinery, pp. 6-1 to 6-23. Meeting held at Naval Postgraduate School, Monterey, California, 22-26 September 1975.
4. Shreeve R. P., McGuire A. G., and Hammer J. A., "Calibration of a Two Probe Synchronized Sampling Technique for Measuring Flows Behind Rotors", paper to be presented at IEEE, Eighth International Congress in Instrumentation in Aerospace Simulation Facilities, Naval Postgraduate School, Monterey, September 24-26 1979. Published as IEEE ICIASF Record of Proceedings.

APPENDIX I

LISTING OF VDR

07/08/79 18.43.34

FILE: VDR FORTRAN P1

N P S

```

C START OF VDR
CT    INTEGER A(6)
CT    IASC=0
CT    IAC=0
CT    DIMENSION ALF(10),PHI(10),XA(40),YA(40),
121    1ZA(40,40),XZ(40),YZ(40),Z3(40,40),XAX(40),YAX(40),
122    2ZAX(40,40),X3X(40),Y3X(40),Z3X(40,40)
119    FORMAT(10)
131    FORMAT(F7.1)
130    FORMAT(F5.1)
120    FORMAT(F8.5)
132    FORMAT(F10.5)
135    FORMAT(F15.5)
136    FORMAT(F17.5)
C READ PROBE CALIBRATION DATA
READ(2,119) XA,NY
DO 121 I=1,NX
121    READ(2,130) XA(I)
DO 122 I=1,NY
122    READ(2,130) YA(I)
DO 123 I=1,NX
DO 123 J=1,NY
123    READ(2,120) ZA(I,J)
DO 221 I=1,NX
221    READ(2,130) XZ(I)
DO 222 I=1,NY
222    READ(2,130) YZ(I)
DO 223 I=1,NX
DO 223 J=1,NY
223    READ(2,120) Z3(I,J)
C TRANSFORM CALIBRATION MATRICES
DO 224 I=1,NY
224    XAX(I)=XA(I)
DO 225 I=1,NX
225    YAX(I)=YA(I)
DO 226 I=1,NY
DO 226 J=1,NX
226    ZAX(I,J)=ZA(I,J)
DO 227 I=1,NX
227    XEX(I)=XZ(I)
DO 228 I=1,NX
228    YEX(I)=YZ(I)
DO 229 I=1,NX
DO 229 J=1,NY
229    ZEX(I,J)=Z3(I,J)
C PROBE SETTINGS
YPA=C.C
YPE=55.
XPA=0.0
XPC=20.
XPL=-2.
C PROGRAM CONSTANTS
YRLP=-30.
YRLP=30.
YRLN=-30.
XFLC=-30.
XRLP=30.
XRLN=-30.
ICCP5=1
NOCOPS=1
NOSIM=1
ILT=1
ISCAN=1
RELXPS=J.5
C EXPERIMENT SIMULATION
401    FORMAT(F15.4)
193    FLAC(5,401) PT
WRITE(6,401) PT
IF(NCS14.EQ.0) GO TO 500
READ(5,401) PS

```

```

INT00010
INT00020
INTCC030
INT00040
INT00050
INT00060
INT00070
INTCC080
INTCC090
INT00100
INTCC110
INT00120
INT00130
INTCC140
INT00150
INTCC160
INT00170
INT00180
INTCC190
INT00200
INT00210
INT00220
INT00230
INTCC240
INT00250
INTCC260
INT00270
INT00280
INTCC290
INT00300
INTCC310
INTCC320
INT00330
INTCC340
INTCC350
INT00360
INTCC370
INT00380
INTCC390
INTCC400
INT00410
INT00420
INTCC430
INT00440
INT00450
INTCC460
INT00470
INT00480
INT00490
INT00500
INTCC510
INTCC520
INT00530
INTCC540
INT00550
INT00560
INTCC570
INT00580
INTCC590
INT00600
INT00610
INTCC620
INTCC630
INT00640
INTCC650
INT00660
INT00670
INTCC680
INT00690
INTCC700

```

FILE: VOR FORTRAN P1 N P S

```

WRITE(6,401) PS
READ(5,401) ALFA
WRITE(6,401) ALFA
READ(5,401) PHII
WRITE(6,401) PHII
CALL INTPLT(XA,YA,ZA,ALFA,PHII,NX,NY,CPA)
ALFC=ALFA-APC
CALL INTPLT(XA,YA,ZA,ALFC,PHII,NX,NY,CPC)
ALFD=ALFA-APD
CALL INTPLT(XA,YA,ZA,ALFD,PHII,NX,NY,CPD)
PHIB=PHII-YPB
CALL INTPLT(XB,YB,ZB,ALFA,PHIB,NX,NY,CPB)
FOYN=PT-PS
PPA=CPA*POYN+PS
PPB=CPB*POYN+PS
PPC=CPC*POYN+PS
PPD=CPD*POYN+PS
C READ MEASUREMENTS DATA
IF(INDS.EQ.1) GO TO 501
50C READ(5,135) PPA
WRITE(6,135) PPA
READ(5,135) PPB
WRITE(6,135) PPB
READ(5,135) PPC
WRITE(6,135) PPC
READ(5,135) PPD
WRITE(6,135) PPD
501 READ(5,135) PSIN
WRITE(6,135) PSIN
IF(ISCAN.EQ.1) GO TO 181
18C IF(ISCAN.EQ.1000) GO TO 305
IT=1
ICUPS=1
ISCAN=ISCAN+1
FSIN=PSIN+5.0

181 PS=PSIN
PSC=FSIN
PST=PS
C CALCULATES PRESSURE COEFFICIENTS
30C POYN=PT-PS
CPA=(PPA-PS)/POYN
CPB=(PPB-PS)/POYN
CPC=(PPC-PS)/POYN
CPD=(PPD-PS)/POYN
C CORRECTS PS ASSUMPTION TO ENSURE CP ARE IN CALIBRATION RANGE
IF(MOCTPS.EQ.2) GO TO 301
ZAMAX=-10000.
CALL MAXXY(ZA,ZAMAX,NX,NY)
IF(CPA.GT.ZAMAX) PSC=1.01*PS
IF(CPC.GT.ZAMAX) PSC=1.01*PS
IF(CPD.GT.ZAMAX) PSC=1.01*PS
ZEMAX=-10000.
CALL MAXXY(ZB,ZEMAX,NX,NY)
IF(CPB.GT.ZEMAX) PSC=1.01*PS
ZAMIN=10000.
CALL MINXY(ZA,ZAMIN,NX,NY)
IF(CPA.LT.ZAMIN) PSC=0.99*PS
IF(CPC.LT.ZAMIN) PSC=0.99*PS
IF(CPD.LT.ZAMIN) PSC=0.99*PS
ZBMIN=10000.
CALL MINXY(ZB,ZBMIN,NX,NY)
IF(CPB.LT.ZBMIN) PSC=0.99*PS
IF(PSC.EQ.PST) GO TO 301
ICOPS=ICUPS+1
IF(ICOPS.GT.10) GO TO 180
PS=PSC
PST=PSC
GO TO 300
C CALCULATES THE ALF & PHI ANGLES FOR 'I' & 'II'

```

INT00710
 INT00720
 INT00730
 INT00740
 INT00750
 INT00760
 INT00770
 INT00780
 INT00790
 INT00800
 INT00810
 INT00820
 INT00830
 INT00840
 INT00850
 INT00860
 INT00870
 INT00880
 INT00890
 INT00900
 INT00910
 INT00920
 INT00930
 INT00940
 INT00950
 INT00960
 INT00970
 INT00980
 INT00990
 INT01000
 INT01010
 INT01020
 INT01030
 INT01040
 INT01050
 INT01070
 INT01080
 INT01090
 INT01100
 INT01110
 INT01120
 INT01130
 INT01140
 INT01150
 INT01160
 INT01170
 INT01180
 INT01190
 INT01200
 INT01210
 INT01220
 INT01230
 INT01240
 INT01250
 INT01260
 INT01270
 INT01280
 INT01290
 INT01300
 INT01310
 INT01320
 INT01330
 INT01340
 INT01350
 INT01360
 INT01370
 INT01380
 INT01390
 INT01400

FILE: VDR FCRTAN PI N D S

```

301 CALL INTSCS(YPA,YPB,YPLC,YFUP,YKIN,
1CPA,CPC,ALF,PHI,AA,YA,ZA,
2XA,YE,AE,AX,YAX,ZAX,XEX,YEX,ZEX,NX,NY,IEPS)
IEPS1=IEPS
ALF1=ALF(1)
ALF2=ALF(2)
PHI1=PHI(1)
PHI2=PHI(2)
C CALCULATES TWO ALF & PHI ANGLES FOR '1' & '111'
CALL INTSCS(XPA,XPC,XPLD,XFUP,XKIN,
1CPA,CPC,PHI,ALF,XAX,YAX,ZAX,
2XAX,YAX,ZAX,AX,YA,ZA,XA,YE,ZA,NX,NY,IEPS)
IEPS2=IEPS
ALF3=ALF(1)
ALF4=ALF(2)
PHI3=PHI(1)
PHI4=PHI(2)
C SELECTS THE PROPER ALF & PHI ANGLES OUT OF THE FOUR VALUES
FALF=((ALF1+ALF2+ALF3+ALF4)-AMAX1(ALF1,ALF2,ALF3,
1ALF4)-AMIN1(ALF1,ALF2,ALF3,ALF4))/2
FPHI=((PHI1+PHI2+PHI3+PHI4)-AMAX1(PHI1,PHI2,PHI3,PHI4)
1-AMIN1(PHI1,PHI2,PHI3,PHI4))/2
C CALCULATES IEPS FROM DATA OF POSITION IV
ALFON=FALF-XPD
CALL INTFLT(XA,YA,ZA,ALFON,FPHI,NX,NY,CPU)
ALFON=FALF-XPC
CALL INTFLT(XA,YA,ZA,ALFON,FPHI,NX,NY,CPC)
PSN=((PCP-CPC-PRD-CPC)/(CPU-CPC))
C CONVERGENCE TESTS
EPSPS=.33*(PSN-PS)/PS
EPSPSC=.0000000009*(PT**2.0)-.00000098*PT
IF(IEPS1-.0000000009*(PT**2.0)-.00000006*PT
1IF(IEPS2-.0000000009*(PT**2.0)-.00000006*PT
2IF(IEPS3-.0000000009*(PT**2.0)-.00000006*PT
3IF(IEPS4-.0000000009*(PT**2.0)-.00000006*PT
4GO TO 310
GO TO 303
11T=11T+1
IF(11T.67.10) GO TO 180
PS=PS+RELAPS*(PSN-PS)
FSC=PS
PST=PS
GO TO 300
303 WRITE(15,174) FALF
171 FFORMAT(15,175) VELOCITY YAW IS' ,F15.2)
WRITE(15,175) FPHI
172 FFORMAT(15,176) VELOCITY PITCH IS' ,F15.2)
WRITE(15,176) FSC
173 FFORMAT(15,177) STATIC PRESSURE IS' ,F15.3)
WRITE(15,177) PST
174 FFORMAT(15,178) TOTAL PRESSURE IS' ,F15.3)
AM=SLFT(11T/PSN)**0.285714-1.0)*5.0)
WRITE(15,178) AM
175 FFORMAT(15,179) ARCH NUMBER IS' ,F15.5)
CT CALL IACLN(15)
CT VIRTIM=(A15)-1A5)/76800
CT CPL=(A16)-1A6)/76800
CT WRITE(15,450) VIRTIM
450 FFORMAT(15,451) VIRTUAL TIME IS' ,F15.5)
CT WRITE(15,451) CPU
451 FFORMAT(15,452) CPU IS' ,F15.5)
CT 1A5C=A(5)
CT 1A6C=A(6)
CT GO TO 193
305 WRITE(15,207)
307 FFORMAT(15,208) SCANNED 1000 TIMES'
GO TO 193
END
SUBROUTINE INTSCS(XPA,XPC,XPLD,XFUP,XKIN,
1HT1,HT2,RES1,RES2,X1,Y1,Z1,
2X2,Y2,Z2,X3,Y3,Z3,X4,Y4,Z4,N1,N2,IEPS)
DIMENSION RES1(10),RES2(10),X1(40),Y1(40),

```

INTO1410
 INTO1420
 INTO1430
 INTO1440
 INTO1450
 INTO1460
 INTO1470
 INTO1480
 INTO1490
 INTO1500
 INTO1510
 INTO1520
 INTO1530
 INTO1540
 INTO1550
 INTO1560
 INTO1570
 INTO1580
 INTO1590
 INTO1600
 INTO1610
 INTO1620
 INTO1630
 INTO1640
 INTO1650
 INTO1660
 INTO1670
 INTO1680
 INTO1690
 INTO1700
 INTO1710
 INTO1720
 INTO1730
 INTO1740
 INTO1750
 INTO1760
 INTO1770
 INTO1780
 INTO1790
 INTO1800
 INTO1810
 INTO1820
 INTO1830
 INTO1840
 INTO1850
 INTO1860
 INTO1870
 INTO1880
 INTO1890
 INTO1900
 INTO1910
 INTO1920
 INTO1930
 INTO1940
 INTO1950
 INTO1960
 INTO1970
 INTO1980
 INTO1990
 INTO2000
 INTO2010
 INTO2020
 INTO2030
 INTO2040
 INTO2050
 INTO2060
 INTO2070
 INTO2080
 INTO2090
 INTO2100

FILE: VDR

FORTRAN P1

N P

S

```

121(40,40),X2(40),Y2(40),Z2(40,40),X3(40),Y3(40),
223(40,40),X4(40),Y4(40),Z4(40,40)
RES1(1)=100.
RES1(2)=5000.
RES2(1)=9000.
RES2(2)=9000.
IEPS=1
ISL=1
ISP=1
CAR=1.
AR2R=AR1N
GO TO 152
150 AR2R=AR2R+CAR
AR2RJ=AR2R
152 ARM1=AR2R-ARP1
ARM2=AR2R-ARP2
C CHECK FOR LOWER CALIBRATION RANGE
IF(ARM1.LT.ARL) GO TO 150
IF(ARM2.LT.ARLC) GO TO 150
K=1
C CALCULATES INITIAL PENETRATION POINTS
CALL PENPTS(N1,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJR=ARRES(2)
CALL PENPTS(N1,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBJL=ARRES(1)
RBJR=ARRES(2)
C CALCULATES SUCCESSIVE PENETRATION POINTS
DO 140 I=1,10000
AR2R=AR2R+CAR
ARM1=AR2R-ARP1
ARM2=AR2R-ARP2
C CHECK FOR UPPER CALIBRATION RANGE
IF(ARM1.GT.ARUP) GO TO 195
IF(ARM2.GT.ARUP) GO TO 195
CALL PENPTS(N1,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJR=ARRES(2)
CALL PENPTS(N1,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBIL=ARRES(1)
RBIR=ARRES(2)
IF(RAJL.EQ.1000.) ISL=10
IF(RBJL.EQ.100.) ISL=10
IF(RAJR.EQ.1000.) ISR=10
IF(RBJR.EQ.1000.) ISR=10
IF(RAIL.EQ.1000.) ISL=10
IF(RBIL.EQ.1000.) ISL=10
IF(RAIR.EQ.1000.) ISR=10
IF(RBIR.EQ.1000.) ISR=10
C CHECK FOR DIRECT HIT BY LEFT INTERSECTION,EVALUATE IF REQUIRED
IF(ISL.NE.10) GO TO 164
ISL=1
GO TO 183
164 IF(RAIL.NE.RBIL) GO TO 180
RES1(K)=RBIL
RES2(K)=AR2R
IF(K.EQ.2) GO TO 155
K=2
GO TO 133
C CHECK FOR INTERMEDIATE LEFT INTERSECTION,EVALUATE IF REQUIRED
180 IF(ISL.NE.10) GO TO 160
ISL=1
GO TO 183
160 IF((RAJL-RBJL)/(RAIL-RBIL).GT.C.O) GO TO 183
AA=(RA2R-A2R)/(RAJL-RAJL)
BA=AR2R-ARAIL
AB=(AR2RJ-AR2R)/(RBJL-RBIL)
BJ=AR2R-ARBIL
RES1(K)=(AA-AB)/(AA-AB)
RES2(K)=AA*RES1(K)+BA

```

```

INTC2110
INTC2120
INTC2130
INTC2140
INTC2150
INTC2160
INTC2170
INTC2180
INTC2190
INTC2200
INTC2210
INTC2220
INTC2230
INTC2240
INTC2250
INTC2260
INTC2270
INTC2280
INTC2290
INTC2300
INTC2310
INTC2320
INTC2330
INTC2340
INTC2350
INTC2360
INTC2370
INTC2380
INTC2390
INTC2400
INTC2410
INTC2420
INTC2430
INTC2440
INTC2450
INTC2460
INTC2470
INTC2480
INTC2490
INTC2500
INTC2510
INTC2520
INTC2530
INTC2540
INTC2550
INTC2560
INTC2570
INTC2580
INTC2590
INTC2600
INTC2610
INTC2620
INTC2630
INTC2640
INTC2650
INTC2660
INTC2670
INTC2680
INTC2690
INTC2700
INTC2710
INTC2720
INTC2730
INTC2740
INTC2750
INTC2760
INTC2770
INTC2780
INTC2790
INTC2800

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FILE: VDR          FORTRAN 91          N    P    S
      IF(K.EQ.2) GO TO 155
      K=2
C CHECK FOR DIRECT HIT OR RIGHT INTERSECTION, EVALUATE IF REQUIRED
183 IF (ISR.NE.10) GO TO 161
      ISR=1
      GO TO 163
161 IF (RAIR.NE.RAIR) GO TO 182
      RES1(K)=RAIR
      RES2(K)=RAIR
      IF(K.EQ.2) GO TO 155
      K=2
      GO TO 163
C CHECK FOR INTERMEDIATE RIGHT INTERSECTION, EVALUATE IF REQUIRED
182 IF (ISR.NE.10) GO TO 162
      ISR=1
      GO TO 163
162 IF ((RAJR-REJR)/(RAIR-RAIR).GT.0.0) GO TO 163
      AA=(AF2RJ-AR2R)/(RAJR-RAIR)
      EA=AR2R-AA*RAIR
      AB=(AF2RJ-AR2R)/(RAJR-RAIR)
      RB=AR2R-AB*RAIR
      RES1(K)=(ES-PA)/(AA-AB)
      RES2(K)=AA*RES1(K)+BA
      IF(K.EQ.2) GO TO 155
      K=2
C RE-INITIATE
163 AR2RJ=AR2R
      RAJL=RAIL
      RAJR=RAIR
      RBIL=RBIL
      RBJR=RBIR
140 WRITE(6,210)
210 FORMAT(' LOOP 140 THROUGH, NO POINTS FOUND')
      GO TO 155
195 IF (RES1(1).EQ.9000.0) GO TO 191
      IF (RES1(2).EQ.9000.0) GO TO 191
      IF (RES2(1).EQ.9000.0) GO TO 191
      IF (RES2(2).EQ.9000.0) GO TO 191
      GO TO 155
C EVALUATION OF INTERSECTIONS WHEN CURVES ARE ALMOST TANGENT
191 YG=0.0
      IEPS=2
      CALL PENPTS(12,N1,X3,Y3,Z3,HT1,YG0,ARRES)
      R1=ABS(ARRES(2)-ARRES(1))/2
      CALL PENPTS(12,N1,X4,Y4,Z4,HT2,YG0,ARRES)
      R2=ABS(ARRES(2)-ARRES(1))/2
      RES2(1)=((R1**2)-(R2**2)+(ARP2**2))/(2.0*ARP2)
      RES2(2)=RES2(1)
      RES1(1)=SIGN(ABS((R1**2)-(RES2(1)**2)))
      RES1(2)=-RES1(1)
155 RETURN
      END
      SUBROUTINE PENPTS(IX,NY,X,Y,Z,HT,YG,XR)
      DIMENSION Y(40),Z(40),ZC(40),XC(40),XR(10)
      IA=1
C SEARCH FOR J OF LOWER Y LINE
      DO 101 I=1,NY
101 IF (Y(I).GE.YG) GO TO 102
102 CONTINUE
      J=I-1
C COARSE SEARCH FOR ZERO PASS
C NEXT 4 LINES ARE EXECUTED IN FIRST SEARCH ONLY
      YC=(YG-Y(J))/(Y(J+1)-Y(J))
      ZC(1)=(Z(I,J+1)-Z(I,J))*YC+Z(I,J)
      IF (ZX(I).EQ.HT) GO TO 107
      I3=2
112 DO 103 I=1,IX
      ZX(I)=(Z(I,J+1)-Z(I,J))*YC+Z(I,J)
      ZM=(Z(I,J+1)-Z(I-1,J))*(YG-Y(J))/(Y(J+1)-Y(J))+Z(I-1,J)
      IF (ZX(I).EQ.HT) GO TO 108

```

```

INTC2810
INT02820
INTC2820
INT02840
INTC2850
INT02860
INTC2870
INT02880
INTC2890
INT02900
INTC2910
INTC2920
INT02930
INTC2940
INT02950
INTC2960
INTC2970
INT02980
INTC2990
INT03000
INT03010
INTC3020
INTC3030
INT03040
INTC3050
INT03060
INT03070
INTC3080
INT03090
INT03100
INT03110
INT03120
INTC3130
INTC3140
INTC3150
INTC3160
INT03170
INT03180
INTC3190
INTC3200
INTC3210
INT03220
INTC3230
INTC3240
INT03250
INT03260
INT03270
INT03280
INTC3290
INT03300
INT03310
INTC3320
INT03330
INT03340
INTC3350
INTC3360
INTC3370
INT03380
INT03390
INTC3400
INT03410
INT03420
INTC3430
INT03440
INTC3450
INTC3460
INTC3470
INTC3480
INT03490
INT03500

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FILE: VOP FORTRAN P1 N P S

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103 IF((ZX(I-1)-HT)/(ZX(I)-HT).LT.0.0) GO TO 104
CONTINUE
C CALCULATION OF PENETRATIONS IN EITHER TRIANGLE
104 XM=X(I-1)+(X(I)-X(I-1))*(YG-Y(J))/(Y(J+1)-Y(J))
IF(ZM.EQ.HT) GO TO 105
IF((ZX(I)-HT)/(ZM-HT).LT.0.0) GO TO 105
ZJ=ABS(Y-Y(J))+ABS(ZX(I-1)-HT)
XS=X(I-1)+(XM-X(I-1))*ABS(ZX(I-1)-HT)/ZJ
GO TO 110
105 XS=XM+(X(I)-XM)*ABS(ZM-HT)/(ABS(ZM-HT)+ABS(ZX(I)-HT))
GO TO 110
C LOGICAL PENETRATIONS ACCUMULATION
107 XR(1)=X(I)
I=1
GO TO 113
108 XR(IR)=X(I)
GO TO 111
110 XR(IR)=XS
111 IF(IR.EQ.2) GO TO 114
IR=2
IR=IR+1
GO TO 114
116 IF(IR.EQ.1) GO TO 117
XR(2)=1000.0
GO TO 114
117 XR(1)=1000.0
XR(2)=1000.0
114 RETURN
END
SUBROUTINE INTPL(X,Y,Z,XG,YG,AX,NY,ZRES)
C LINEAR INTERPOLATION ON CALIBRATION SURFACE TO EVALUATE
C CP VALUE AT CO-ORDINATES XG,YG. THE RESULT RETURNED IS ZRES
DIMENSION X(40),Y(40),Z(40,40)
C SEARCH FOR I OF LEFT X LINE
DO 1 IC=1,NX
IF(X(IC).GE.XG) GO TO 2
CONTINUE
1 IC=IC-1
C SEARCH FOR J OF LOWER Y LINE
DO 3 JC=1,NY
IF(Y(JC).GE.YG) GO TO 4
CONTINUE
3 JC=JC-1
4 AL=(Y(J+1)-Y(J))/(X(I+1)-X(I))
BL=Y(J)-AL*X(I)
YCR=(AL*XG)+BL
IF(YG.EQ.YCR) GO TO 7
IF(YG.GT.YCR) GO TO 5
C RESULTING Z IS IN LOWER TRIANGLE
X3=X(I+1)
Y3=Y(J)
Z3=Z(I+1,J)
GO TO 6
C RESULTING Z IS IN UPPER TRIANGLE
5 X3=X(I)
Y3=Y(J+1)
Z3=Z(I,J+1)
C GENERAL CALCULATION: GOOD FOR BOTH TRIANGLES
6 X1=X(I)
Y1=Y(J)
Z1=Z(I,J)
X2=X(I+1)
Y2=Y(J+1)
Z2=Z(I+1,J+1)
AP=((Z1-Z3)*(Y1-Y2)-(Z1-Z2)*(Y1-Y3))/((X1-X3)*(Y1-Y2)-(X1-X2)
1*(Y1-Y3))
BP=((Z1-Z2)-AP*(X1-X2))/(Y1-Y2)
CP=Z1-AP*X1-BP*Y1
ZRES=AP*XG+BP*Y1+CP

```

INTO3510
 INTO3520
 INTO3530
 INTO3540
 INTO3550
 INTO3560
 INTO3570
 INTO3580
 INTO3590
 INTO3600
 INTO3610
 INTO3620
 INTO3630
 INTO3640
 INTO3650
 INTO3660
 INTO3670
 INTO3680
 INTO3690
 INTO3700
 INTO3710
 INTO3720
 INTO3730
 INTO3740
 INTO3750
 INTO3760
 INTO3770
 INTO3780
 INTO3790
 INTO3800
 INTO3810
 INTO3820
 INTO3830
 INTO3840
 INTO3850
 INTO3860
 INTO3870
 INTO3880
 INTO3890
 INTO3900
 INTO3910
 INTO3920
 INTO3930
 INTO3940
 INTO3950
 INTO3960
 INTO3970
 INTO3980
 INTO3990
 INTO4000
 INTO4010
 INTO4020
 INTO4030
 INTO4040
 INTO4050
 INTO4060
 INTO4070
 INTO4080
 INTO4090
 INTO4100
 INTO4110
 INTO4120
 INTO4130
 INTO4140
 INTO4150
 INTO4160
 INTO4170
 INTO4180
 INTO4190
 INTO4200

611492

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INTC421J
INTC422J
INTC423C
INTC424J
INTC425J
INTC426J
INTC427J
INTC428C
INTC429J
INTC430J
INTC431J
INTC432J
INTC433J
INTC434J
INTC435J
INTC436J
INTC437J
INTC438J
INTC439J
INTC440J
INTC441J
INTC442J
INTC443J
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APPENDIX 2

LISTING OF SWVDR

07/08/75 12.45.15

FILE: SAVER FORTRAN PL

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P

S

C START OF SAVOR

119 DIMENSION ALF(10),PHI(10),XA(40),YA(40),
120 1ZA(40,40),XB(40),YB(40),ZB(40,40),XAX(40),YAX(40),
121 2ZA(40,40),XAX(40),YBX(40),ZBX(40,40)

119 FORMAT(215)
121 FORMAT(F7.1)
120 FORMAT(F5.1)
122 FORMAT(F8.5)
123 FORMAT(F10.5)
124 FORMAT(F15.5)
125 FORMAT(F17.5)

C READ PROJECT CALIBRATION DATA

121 READ(2,119) IX,IY
DO 121 I=1,IX
READ(2,120) XA(I)

121 CONTINUE
DO 122 I=1,NY
READ(2,120) YA(I)

122 CONTINUE
DO 123 I=1,NX
DO 123 J=1,IY
READ(2,120) ZA(I,J)

123 CONTINUE
DO 221 I=1,NX
READ(2,120) XB(I)

221 CONTINUE
DO 222 I=1,NY
READ(2,120) YB(I)

222 CONTINUE
DO 223 I=1,NX
DO 223 J=1,IY
READ(2,120) ZB(I,J)

223 CONTINUE
C TRANSFORM CALIBRATION MATRICES

224 DO 224 I=1,NY
XAX(I)=YA(I)

225 DO 225 I=1,NX
YAX(I)=XA(I)

226 DO 226 J=1,IY
DO 226 I=1,NX
ZAX(I,J)=ZB(J,I)

227 DO 227 I=1,NY
XBX(I)=YB(I)

228 DO 228 I=1,NX
DO 228 J=1,IY
ZBX(I,J)=ZB(J,I)

C FREQUENCY SETTINGS

YPA=0.0
YPB=55.
XPA=0.0
XPC=20.
XPD=-20.

C PROGRAM CONSTANTS

YPLD=-30.
YRUP=30.
YRIN=-30.
XRLD=-30.
XRLP=30.
XRIN=-30.
ICOPS=1
ACCCFS=2
NOSIM=2
IIT=1
ISCAN=1
RELXPS=0.5

C EXPERIMENT SIMULATION

193 CONTINUE
401 FORMAT(F15.4)

INT00010
INT00020
INT00030
INT00040
INT00050
INT00060
INT00070
INT00080
INT00090
INT00100
INT00110
INT00120
INT00130
INT00140
INT00150
INT00160
INT00170
INT00180
INT00190
INT00200
INT00210
INT00220
INT00230
INT00240
INT00250
INT00260
INT00270
INT00280
INT00290
INT00300
INT00310
INT00320
INT00330
INT00340
INT00350
INT00360
INT00370
INT00380
INT00390
INT00400
INT00410
INT00420
INT00430
INT00440
INT00450
INT00460
INT00470
INT00480
INT00490
INT00500
INT00510
INT00520
INT00530
INT00540
INT00550
INT00560
INT00570
INT00580
INT00590
INT00600
INT00610
INT00620
INT00630
INT00640
INT00650
INT00660
INT00670
INT00680
INT00690
INT00700

FILE: SWDOR FCRTRAN P1

N P

S

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READ(5,401) PT
WRITE(6,401) PT
IF(ICSIN.EQ.2) GO TO 500
READ(5,401) PS
WRITE(6,401) PS
READ(5,401) ALFA
WRITE(6,401) ALFA
READ(5,401) PHII
WRITE(6,401) PHII
CALL INTPLT(XA,YA,ZA,ALFA,PHII,NX,NY,CPA)
ALFC=ALFA-APC
CALL INTFLT(XA,YA,ZA,ALFC,PHII,NX,NY,CPC)
ALFE=ALFA-APC
CALL INTFLT(XA,YA,ZA,ALFE,PHII,NX,NY,CPC)
PHIB=PHII-YPB
CALL INTFLT(XB,YB,ZB,ALFA,PHIB,NX,NY,CDB)
PDYN=PT-PS
PPA=CPA*PDYN+PS
PFB=CFB*PDYN+PS
PPC=CPC*PDYN+PS
PFC=CPD*PDYN+PS
C READ MEASUREMENTS DATA
IF(INDSI4.EQ.1) GO TO 501
500 READ(5,135) PPA
WRITE(6,136) PPA
READ(5,135) PFB
WRITE(6,136) PFB
READ(5,135) PPC
WRITE(6,136) PPC
READ(5,135) PFC
WRITE(6,136) PFC
501 READ(5,135) PSIN
WRITE(6,136) PSIN
IF(ISCAN.EQ.1) GO TO 181
180 IF(ISCAN.EQ.1000) GO TO 305
II=1
ICCP=1
ISCAN=ISCAN+1
PSIN=PSIN+5.0
WRITE(6,136) PSIN
181 CONTINUE
PS=PSIN
PSC=PSIN
PST=PS
C CALCULATES PRESSURE COEFFICIENTS
300 CONTINUE
PDYN=PT-PS
CPA=(PPA-PS)/PDYN
CFB=(PFB-PS)/PDYN
CPC=(PPC-PS)/PDYN
CPD=(PFC-PS)/PDYN
C CORRECTS PS ASSUMPTION TO ENSURE CF ARE IN CALIBRATION RANGE
IF(INDCPS.EQ.2) GO TO 301
ZAMAX=-10000.
CALL MAXARY(ZA,ZAMAX,NX,NY)
IF(CPA.GT.ZAMAX) PSC=1.01*PS
IF(CFB.GT.ZAMAX) PSC=1.01*PS
IF(CPD.GT.ZAMAX) PSC=1.01*PS
ZBMAX=-10000.
CALL MAXARY(ZB,ZBMAX,NX,NY)
IF(CPB.GT.ZBMAX) PSC=1.01*PS
ZAMIN=10000.
CALL MINARY(ZA,ZAMIN,NX,NY)
IF(CPA.LT.ZAMIN) PSC=0.99*PS
IF(CPC.LT.ZAMIN) PSC=0.99*PS
IF(CPD.LT.ZAMIN) PSC=0.99*PS
ZBMIN=10000.
CALL MINARY(ZB,ZBMIN,NX,NY)
IF(CPB.LT.ZBMIN) PSC=0.99*PS
IF(PSC.EQ.PST) GO TO 301

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INTC0710
INTC0720
INTC0730
INTC0740
INTC0750
INTC0760
INTC0770
INTC0780
INTC0790
INTC0800
INTC0810
INTC0820
INTC0830
INTC0840
INTC0850
INTC0860
INTC0870
INTC0880
INTC0890
INTC0900
INTC0910
INTC0920
INTC0930
INTC0940
INTC0950
INTC0960
INTC0970
INTC0980
INTC0990
INTC1000
INTC1010
INTC1020
INTC1030
INTC1040
INTC1050
INTC1060
INTC1070
INTC1080
INTC1090
INTC1100
INTC1110
INTC1120
INTC1130
INTC1140
INTC1150
INTC1160
INTC1170
INTC1180
INTC1190
INTC1200
INTC1210
INTC1220
INTC1230
INTC1240
INTC1250
INTC1260
INTC1270
INTC1280
INTC1290
INTC1300
INTC1310
INTC1320
INTC1330
INTC1340
INTC1350
INTC1360
INTC1370
INTC1380
INTC1390
INTC1400

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FILE: SWVER FORTRAN P1

N P

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      ICOPS=ICOPS+1
      IF (ICOPS.GT.10) GO TO 180
      PS=PSC
      PST=PSC
      GO TO 300
301 CONTINUE
      C CALCULATES THE ALF & PHI ANGLES FOR 'I' & 'II'
      CALL INTSCS(XPA,YPA,XRL,YRUP,YKIN,
      1CPA,CPS,ALF,PHI,XA,YA,ZA,
      2XB,YR,ZB,XB,YAX,ZAX,XBX,YHX,ZBX,NX,NY)
      ALF1=ALF(1)
      ALF2=ALF(2)
      PHI1=PHI(1)
      PHI2=PHI(2)
      C CALCULATES THE ALF & PHI ANGLES FOR 'I' & 'III'
      CALL INTSCS(XPA,XPC,XRLD,XRUP,XRIN,
      1CPA,CPC,PHI,ALF,YAX,YAX,ZAX,
      2XAX,YAX,ZAX,XA,YA,ZA,XA,YA,ZA,NY,NX)
      ALF3=ALF(1)
      ALF4=ALF(2)
      PHI3=PHI(1)
      PHI4=PHI(2)
      C SELECTS THE PROPER ALF & PHI ANGLES OUT OF THE FOUR VALUES
      FALF=((ALF1+ALF2+ALF3+ALF4)-AMAX1(ALF1,ALF2,ALF3,
      1ALF4))-AMIN1(ALF1,ALF2,ALF3,ALF4))/2
      FPHI=((PHI1+PHI2+PHI3+PHI4)-AMAX1(PHI1,PHI2,PHI3,PHI4)
      1-AMIN1(PHI1,PHI2,PHI3,PHI4))/2
      C CALCULATES THE PS FROM DATA OF POSITION D AND CORRECTS PT
      ALFEN=FALF-XPD
      CALL INTPT(XA,YA,ZA,ALFEN,FPHI,NX,NY,CPC)
      ALFEN=FALF-XPC
      CALL INTPLT(XA,YA,ZA,ALFEN,FPHI,NX,NY,CPC)
      PSN=(CPC*CPJ-PPJ*CPC)/(CPU-CPC)
      WRITE(5,11) IIT,FALF,FPHI,PSN
907 FORMAT(' ITERATION VALUES',I5,10X,2F6.2,F10.2)
911 C CONVERGENCE TESTS
      EPSPS=ABS((PSN-PS)/PS)
      EPSPSG=.000070JOCU77*(PT**2.0)-.00000098*PT
      IF (ICPS1.EQ.2) EPSPSG=.0000000009*(PT**2.0)-.00000038*PT
      IF (IEPS2.EQ.2) EPSPSG=.0000000009*(PT**2.0)-.00000000*PT
      IF (IEPS3.GT.EPSPSG) GO TO 310
      GO TO 300
310 CONTINUE
      IIT=IIT+1
      IF (IIT.GT.10) GO TO 180
      PS=PS+RELXPS*(PSN-PS)
      PSC=PS
      PST=PS
      GO TO 300
303 WRITE(5,11) FALF
171 FORMAT('01 VELOCITY YAW IS',F15.2)
172 WRITE(5,12) FPHI
      FORMAT('01 VELOCITY PITCH IS',F15.2)
173 WRITE(5,13) PSN
      FORMAT('01 STATIC PRESSURE IS',F15.3)
174 WRITE(5,14) PT
      FORMAT('01 TOTAL PRESSURE IS',F15.3)
      AM=SCFT((PT/PSN)**0.285714-1.0)*5.0)
      WRITE(5,15) AM
175 FORMAT('01 MACH NUMBER IS',F15.5)
      GO TO 193
305 WRITE(5,307)
307 FORMAT(' SCANNED 1000 TIMES')
      GO TO 193
      END
      SUBROUTINE INTSCS(ARP1,ARP2,ARLD,ARUP,APIN,
      1HT1,HT2,RES1,RES2,XA,YA,ZA,
      2X2,Y2,Z2,X3,Y3,Z3,X4,Y4,Z4,N1,N2)
      DIMENSION RES1(10),RES2(10),A=RES(10),X1(40),Y1(40),
      1Z1(40,40),X2(40),Y2(40),Z2(40,40),X3(40),Y3(40),

```

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INTC1410
INTC1420
INTC1430
INTC1440
INTC1450
INTC1460
INTC1470
INTC1480
INTC1490
INTC1500
INTC1510
INTC1520
INTC1530
INTC1540
INTC1550
INTC1560
INTC1570
INTC1580
INTC1590
INTC1600
INTC1610
INTC1620
INTC1630
INTC1640
INTC1650
INTC1660
INTC1670
INTC1680
INTC1690
INTC1700
INTC1710
INTC1720
INTC1730
INTC1740
INTC1750
INTC1760
INTC1770
INTC1780
INTC1790
INTC1800
INTC1810
INTC1820
INTC1830
INTC1840
INTC1850
INTC1860
INTC1870
INTC1880
INTC1890
INTC1900
INTC1910
INTC1920
INTC1930
INTC1940
INTC1950
INTC1960
INTC1970
INTC1980
INTC1990
INTC2000
INTC2010
INTC2020
INTC2030
INTC2040
INTC2050
INTC2060
INTC2070
INTC2080
INTC2090
INTC2100

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FILE: SAVCP FORTRAN P1

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P

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22J(40,40),X4(40),Y4(40),Z+(40,40)
RES1(1)=9000.
RES1(2)=9000.
RES2(1)=9000.
RES2(2)=9000.
ISL=1
ISR=1
UAR=1.
AR2R=ARIN
GC TC 152
150 AR2R=AR2R+UAR
AR2RJ=AR2R
152 ARV1=AR2R-ARP1
ARM2=AR2R-ARP2
C CHECK FOR LOWER CALIBRATION RANGE
IF (ARM1.LT.ARL0) GC TC 150
IF (ARM2.LT.ARL0) GC TC 150
K=1
C CALCULATES INITIAL PENETRATION POINTS
CALL PENPTS(N1,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJR=ARRES(2)
CALL PENPTS(N1,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBIL=ARRES(1)
RBJR=ARRES(2)
C CALCULATES SUCCESSIVE PENETRATION POINTS
DO 140 J=1,10000
AP2R=AR2R+UAR
ARM1=AR2R-ARP1
ARM2=AR2R-ARP2
C CHECK FOR UPPER CALIBRATION RANGE
IF (ARM1.GT.ARUP) GC TC 195
IF (ARM2.GT.ARUP) GC TC 195
CALL PENPTS(N1,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJR=ARRES(2)
CALL PENPTS(N1,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBIL=ARRES(1)
RBJR=ARRES(2)
IF (RAJL.EQ.1000.) ISL=10
IF (RAJR.EQ.1000.) ISR=10
IF (RBIL.EQ.1000.) ISL=10
IF (RBJR.EQ.1000.) ISR=10
IF (RAJL.EQ.1000.) ISL=10
IF (RAJR.EQ.1000.) ISR=10
IF (RBIL.EQ.1000.) ISL=10
IF (RBJR.EQ.1000.) ISR=10
C CHECK FOR DIRECT HIT TO LEFT INTERSECTION, EVALUATE IF REQUIRED
IF (ISL.NE.10) GC TO 164
ISL=1
GC TC 183
164 IF (RAJL.NE.RBIL) GO TO 180
RES1(K)=RAJL
RES2(K)=AR2R
IF (K.EQ.2) GO TO 155
K=2
GC TC 183
C CHECK FOR INTERMEDIATE LEFT INTERSECTION, EVALUATE IF REQUIRED
180 IF (ISL.NE.10) GO TO 160
ISL=1
GO TO 183
160 IF ((RAJL-RBIL)/(RAJL-RBIL).GT.0.0) GO TO 183
AA=(AR2RJ-AR2R)/(RAJL-RAJL)
AB=(AR2RJ-AR2R)/(RBIL-RBIL)
BB=AR2R-AB*RBIL
RES1(K)=(AA-AB)/(AA-18)
RES2(K)=AA*RES1(K)+EA
IF (K.EQ.2) GO TO 155
K=2

```

INTC2110
INTC2120
INTC2130
INTC2140
INTC2150
INTC2160
INTC2170
INTC2180
INTC2190
INTC2200
INTC2210
INTC2220
INTC2230
INTC2240
INTC2250
INTC2260
INTC2270
INTC2280
INTC2290
INTC2300
INTC2310
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INTC2380
INTC2390
INTC2400
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INTC2470
INTC2480
INTC2490
INTC2500
INTC2510
INTC2520
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INTC2580
INTC2590
INTC2600
INTC2610
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INTC2670
INTC2680
INTC2690
INTC2700
INTC2710
INTC2720
INTC2730
INTC2740
INTC2750
INTC2760
INTC2770
INTC2780
INTC2790
INTC2800

FILE: SWVR FORTRAN P1 N P S

C CHECK FOR DIRECT HIT ON RIGHT INTERSECTION, EVALUATE IF REQUIRED

183 IF (ISH.NE.10) GO TO 161

ISH=1

GO TO 163

161 IF (RAIR.NE.RBIR) GO TO 182

RES1(K)=R3IR

RES2(K)=R2IR

IF (K.EQ.2) GO TO 183

K=2

GO TO 163

C CHECK FOR INTERMEDIATE RIGHT INTERSECTION, EVALUATE IF REQUIRED

182 IF (ISH.NE.10) GO TO 162

ISH=1

GO TO 163

162 IF ((RAJR-R3JR)/(PAIR-RBIR).GT.0.0) GO TO 163

AA=(AP2FJ-AR2J)/(RAJR-RAIR)

EA=AR2K-AA*RAIR

AB=(AR2J-AR2J)/(RAJR-RAIR)

EB=AR2K-AB*RAIR

RES1(K)=(AB-EA)/(AA-AB)

RES2(K)=AA*RES1(K)+EA

IF (K.EQ.2) GO TO 155

K=2

C RE-INITIATE

163 AR2HJ=AR2H

RAJR=PAIR

RAJR=PAIR

RAJR=PAIR

RAJR=PAIR

RAJR=PAIR

140 C INT INJE

WRITE(6,210)

210 FORMAT(' LJOJ 140 THROUGH, N1 POINTS FOUND')

GO TO 155

195 IF (RES1(1).EQ.9000.0) GO TO 191

IF (RES1(2).EQ.9000.0) GO TO 191

IF (RES2(1).EQ.9000.0) GO TO 191

IF (RES2(2).EQ.9000.0) GO TO 191

GO TO 155

C EVALUATION OF INTERSECTIONS WHEN CURVES ARE ALMOST TANGENT

191 YG=U-U

CALL PENPTS (N2,N1,X3,Y3,Z3,HT1,YG,ARRES)

R1=ABS(ARRES(2)-ARRES(1))/2

CALL PENPTS (N2,N1,X4,Y4,Z4,HT2,YG,ARRES)

R2=ABS(ARRES(2)-ARRES(1))/2

RES2(1)=((R1**2)-(R2**2)+(ARP2**2))/(2.0*ARP2)

RES2(2)=RES2(1)

RES1(1)=SIGN(ABS((R1**2)-(RES2(1)**2)))

RES1(2)=-RES1(1)

155 RETURN

END

SUBROUTINE PENPTS (NX,NY,X,Y,Z,HT,YG,XR)

DIMENSION Y(40),ZX(40),Z(40,40),X(40),XR(10)

IR=1

C SEARCH FOR J OF LOWER Y LINE

DO 101 I=1,NY

IF (Y(I).GE.YG) GO TO 102

101 CONTINUE

J=I-1

C CHASE SCAN FOR ZERO PASS

C NEXT 3 LINES ARE EXECUTED IN FIRST SEARCH ONLY

YC=(Y(I)-Y(J))/(Y(I+1)-Y(J))

ZX(1)=(Z(I,I+1)-Z(I,I))*YC+Z(I,I)

IF (ZX(1).EQ.HT) GO TO 107

IR=2

112 DO 103 I=1B,IX

ZX(1)=(Z(I,I+1)-Z(I,I))*YC+Z(I,I)

Z4=(Z(I,I+1)-Z(I,I))*YC+(Y(I+1)-Y(I))+Z(I,I+1)

IF (ZX(1).EQ.HT) GO TO 108

IF ((ZX(1)-HT)/(ZX(1)-HT).LT.0.0) GO TO 108

103 CONTINUE

INTC2810
INTC2820
INTC2830
INTC2840
INTC2850
INTC2860
INTC2870
INTC2880
INTC2890
INTC2900
INTC2910
INTC2920
INTC2930
INTC2940
INTC2950
INTC2960
INTC2970
INTC2980
INTC2990
INTC3000
INTC3010
INTC3020
INTC3030
INTC3040
INTC3050
INTC3060
INTC3070
INTC3080
INTC3090
INTC3100
INTC3110
INTC3120
INTC3130
INTC3140
INTC3150
INTC3160
INTC3170
INTC3180
INTC3190
INTC3200
INTC3210
INTC3220
INTC3230
INTC3240
INTC3250
INTC3260
INTC3270
INTC3280
INTC3290
INTC3300
INTC3310
INTC3320
INTC3330
INTC3340
INTC3350
INTC3360
INTC3370
INTC3380
INTC3390
INTC3400
INTC3410
INTC3420
INTC3430
INTC3440
INTC3450
INTC3460
INTC3470
INTC3480
INTC3490
INTC3500

FILE: SWVDR FORTRAN P1

N P

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      GO TO 116
C CALCULATION OF PENETRATIONS IN EITHER TRIANGLE
104  XM=X(I-1)+(X(I)-X(I-1))*(YG-Y(J))/(Y(J+1)-Y(J))
      IF(ZM.EJ.HT) GO TO 105
      IF((ZX(I)-HT)/(ZM-HT).LT.0.0) GO TO 105
      DD=ABS(MT-ZM)+ABS(ZX(I-1)-HT)
      XS=(I-1)+(XM-X(I-1))*ABS(ZX(I-1)-HT)/DD
      GO TO 110
105  XS=M+(X(I)-XM)*ABS(ZM-HT)/(ABS(ZM-HT)+ABS(ZX(I)-HT))
      GO TO 110
C LOCAL PENETRATIONS ACCUMULATION
107  XR(1)=X(1)
      I=1
      GO TO 113
108  XR(I2)=X(I)
      GO TO 111
110  XR(I2)=XS
111  IF(I2.EQ.2) GO TO 114
113  IK=2
      IB=I+1
      GO TO 112
116  IF(I2.EQ.1) GO TO 117
      XR(2)=1000.0
      GO TO 114
117  XR(1)=1000.0
      XR(2)=1000.0
114  RETURN
      END
SUBROUTINE INTPLT(X,Y,Z,XG,YG,NX,NY,ZRES)
C LINEAR INTERPOLATION ON CALIP-AT-1 IN SURFACE TO EVALUATE
C CP VALLE AT CO-ORDINATES XG,YG. THE RESULT RETURNED IS ZRES
      DIMENSION A(40),Y(40),Z(40,40)
C SEARCH FOR I OF LEFT X LINE
      DO 1 IC=1,NX
      IF(X(IC).GE.XG) GO TO 2
1    CCNTINJE
      I=IC-1
C SEARCH FOR J OF LOWER Y LINE
      DO 3 JC=1,NY
      IF(Y(JC).GE.YG) GO TO 4
3    CCNTINJE
      J=JC-1
      AL=(Y(J+1)-Y(J))/(X(I+1)-X(I))
      BL=Y(J)-AL*X(I)
      YCR=(AL*XG)+BL
      IF(YG.EQ.YCR) GO TO 7
      IF(YG.GT.YCR) GO TO 5
C RESULTING Z IS IN LOWER TRIANGLE
      X3=X(I+1)
      Y3=Y(J)
      Z3=Z(I+1,J)
      GO TO 6
C RESULTING Z IS IN UPPER TRIANGLE
5    X3=X(I)
      Y3=Y(J+1)
      Z3=Z(I,J+1)
C GENERAL CALCULATION: GOOD FOR BOTH TRIANGLES
6    X1=X(I)
      Y1=Y(J)
      Z1=Z(I,J)
      X2=X(I+1)
      Y2=Y(J+1)
      Z2=Z(I+1,J+1)
      AP=((Z1-Z3)*(Y1-Y2)-(Z1-Z2)*(Y1-Y3))/(X1-X3)*(Y1-Y2)-(X1-X2)
      CP=((Z1-Z2)*(Y1-Y3)-(Z1-Z3)*(Y1-Y2))/(Y1-Y2)
      ZRES=AP*XG+CP*YG+C
      GO TO 100
C RESULTING Z IS ON DIVIDING LINE

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INTC3510
INTC3520
INTC3530
INTC3540
INTC3550
INTC3560
INTC3570
INTC3580
INTC3590
INTC3600
INTC3610
INTC3620
INTC3630
INTC3640
INTC3650
INTC3660
INTC3670
INTC3680
INTC3690
INTC3700
INTC3710
INTC3720
INTC3730
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INTC3780
INTC3790
INTC3800
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INTC3870
INTC3880
INTC3890
INTC3900
INTC3910
INTC3920
INTC3930
INTC3940
INTC3950
INTC3960
INTC3970
INTC3980
INTC3990
INTC4000
INTC4010
INTC4020
INTC4030
INTC4040
INTC4050
INTC4060
INTC4070
INTC4080
INTC4090
INTC4100
INTC4110
INTC4120
INTC4130
INTC4140
INTC4150
INTC4160
INTC4170
INTC4180
INTC4190
INTC4200

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6

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INTC4210
INTC4220
INTC4230
INTC4240
INTC4250
INTC4260
INTC4270
INTC4280
INTC4290
INTC4300
INTC4310
INTC4320
INTC4330
INTC4340
INTC4350
INTC4360
INTC4370
INTC4380
INTC4390
INTC4400
INTC4410
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INTC4230
INTC4240
INTC4250
INTC4260
INTC4270
INTC4280
INTC4290
INTC4300
INTC4310
INTC4320
INTC4330
INTC4340
INTC4350
INTC4360
INTC4370
INTC4380
INTC4390
INTC4400
INTC4410

INTC4260
INTC4270
INTC4280
INTC4290
INTC4300
INTC4310
INTC4320
INTC4330
INTC4340
INTC4350
INTC4360
INTC4370
INTC4380
INTC4390
INTC4400
INTC4410

INTC4310
INTC4320
INTC4330
INTC4340
INTC4350
INTC4360
INTC4370
INTC4380
INTC4390
INTC4400
INTC4410

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INTC4340
INTC4350
INTC4360
INTC4370
INTC4380
INTC4390
INTC4400
INTC4410

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INT04390
INT04400
INT04410

APPENDIX 3

LISTING OF WVDR

07/08/75 16.45.53

FILE: WVLN FORTKAN F1

N P

S

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C START OF WVLN
  DIMENSION ALF(10),PHI(10),XA(40),YA(40),
  1ZA(10,40),XB(40),YB(40),ZP(40,40),XAX(40),YAX(40),
  2ZAX(40,40),XBX(40),ZBX(40,40)
119  FORMAT(2I5)
131  FORMAT(F7.1)
130  FORMAT(F5.1)
120  FORMAT(F5.5)
132  FORMAT(F10.5)
135  FORMAT(F15.5)
136  FORMAT(F17.5)
C READ PROFILE CALIBRATION DATA
  READ(2,119) IA,IY
  DO 121 I=1,IA
    READ(2,120) XA(I)
    CONTINUE
121  DO 122 I=1,IY
    READ(2,120) YA(I)
    CONTINUE
122  DO 123 I=1,IA
    DO 123 J=1,IY
      READ(2,120) ZA(I,J)
      CONTINUE
123  DO 221 I=1,IX
    READ(2,130) XB(I)
    CONTINUE
221  DO 222 I=1,IY
    READ(2,130) YB(I)
    CONTINUE
222  DO 223 I=1,IA
    DO 223 J=1,IY
      READ(2,120) ZB(I,J)
      CONTINUE
223  C TRANSFORM CALIBRATION MATRICES
    DO 224 I=1,IY
      XAX(I)=YA(I)
      DO 225 I=1,IA
        YAX(I)=XB(I)
        DO 226 J=1,IY
          ZAX(I,J)=ZA(I,J)
          DO 227 I=1,IX
            XBX(I)=YE(I)
            DO 228 I=1,IA
              YBX(I)=XB(I)
              DO 229 J=1,IY
                ZBX(I,J)=ZB(I,J)
          CONTINUE
229  C FRCBE SETTINGS
        YPA=C.0
        YPB=55.
        XPA=C.0
        XPC=20.
        XPD=-2.
C PROGRAM CONSTANTS
        YRLC=-30.
        YRLP=30.
        YRLN=-30.
        XRLC=-30.
        XRLP=30.
        XRLN=-30.
        ICCPS=1
        NJCUPS=2
        NOSIM=1
        ITT=1
        ISCAN=1
        RELAXE=J.2
C EXPERIMENT SAVLLSTACN
195  CONTINUE
401  FORMAT(F15.4)

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INT00010
INT00020
INT00030
INT00040
INT00050
INT00060
INT00070
INT00080
INT00090
INT00100
INT00110
INT00120
INT00130
INT00140
INT00150
INT00160
INT00170
INT00180
INT00190
INT00200
INT00210
INT00220
INT00230
INT00240
INT00250
INT00260
INT00270
INT00280
INT00290
INT00300
INT00310
INT00320
INT00330
INT00340
INT00350
INT00360
INT00370
INT00380
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INT00700

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FILE: 4VCR FORTRAN P1 . N P S

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READ(5,401) PT
WRITE(6,401) PT
IF (INCSIN.EQ.2) GO TO 500
READ(5,401) PS
WRITE(6,401) PS
READ(5,401) ALFA
WRITE(6,401) ALFA
READ(5,401) PHII
WRITE(6,401) PHII
CALL INPLT(XA,YA,ZA,ALFA,PHII,NX,NY,CPA)
ALFC=ALFA-XPC
CALL INPLT(XA,YA,ZA,ALFC,PHII,NX,NY,CPC)
ALFD=ALFA-XPD
CALL INPLT(XA,YA,ZA,ALFD,PHII,NX,NY,CPD)
PHIP=PHII-YPS
CALL INPLT(XA,YA,ZA,ALFA,PHIP,NX,NY,CPA)
WRITE(5,402) CPA,CPC,CPD
402 FORMAT(1X,'CP',4F10.5)
PUYN=PT-PS
PPA=CPA*PUYN+PS
PPC=CPC*PUYN+PS
PPD=CPD*PUYN+PS
WRITE(5,403) PPA,PPC,PPD
403 FORMAT(1X,'P',3F10.2)
C READ MEASUREMENTS DATA
IF (INCSIN.EQ.1) GO TO 501
500 READ(5,135) PSA
WRITE(6,135) PSA
READ(5,135) PPB
WRITE(6,135) PPB
READ(5,135) PPC
WRITE(6,135) PPC
READ(5,135) PPD
WRITE(6,135) PPD
501 READ(5,135) PSIN
WRITE(6,135) PSIN
IF (ISCAN.EQ.1) GO TO 181
180 IF (ISCAN.EQ.1000) GO TO 305
IIT=1
ICGPE=1
ISCAN=ISCAN+1
PSIN=PSIN+5.0
WRITE(6,136) PSIN
181 CONTINUE
PS=PSIN
PSC=PS
PST=PS
C CALCULATES PRESSURE COEFFICIENTS
300 CONTINUE
WRITE(5,940) IIT
940 FORMAT(1X,'ITERATION NO. ',15)
PUYN=PT-PS
CPA=(PPA-PS)/PUYN
CPB=(PPB-PS)/PUYN
CPC=(PPC-PS)/PUYN
CPD=(PPD-PS)/PUYN
908 WRITE(5,912) CPA,CPC,CPD
912 FORMAT(1X,'COEFF',4F10.5)
C CORRECTS PRESSURE COEFFICIENTS TO ENSURE CP ARE IN CALIBRATION RANGE
IF (ACCP.EQ.2) GO TO 501
ZAPAX=-10000.
CALL XAXY(ZA,ZAPAX,NX,NY)
IF (CPA.GT.2.51AX) PSC=1.01*PS
IF (CPC.GT.2.51AX) PSC=1.01*PS
IF (CPD.GT.2.51AX) PSC=1.01*PS
ZAPAX=-10000.
CALL XAXY(ZA,ZAPAX,NX,NY)
IF (CPA.GT.2.51AX) PSC=1.01*PS
ZAPIN=10000.

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INT01400

FILE: WCFR FORTRAN P1

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CALL MINARY(ZA,ZAMIN,NX,NY)
IF(CPA.LT.ZAMIN) PSC=0.99*PS
IF(CPC.LT.ZAMIN) PSC=0.99*PS
IF(CPD.LT.ZAMIN) PSC=0.99*PS
ZAMIN=10000.
CALL MINARY(ZB,ZEMIN,NX,NY)
IF(CPB.LT.ZEMIN) PSC=C.99*PS
IF(PSC.EC.PST) GO TO 301
ICLPS=ICLPS+1
963 WRITE(6,564) ICLPS
964 FORMAT(' ICLPS IS',15)
IF(ICLPS.GT.10) GO TO 180
PS=PSC
PST=PSC
920 WRITE(6,521) PSC
921 FORMAT(' PSC IS',F20.5)
GO TO 300
301 CONTINUE
C CALCULATES TWO ALF & PHI ANGLES FOR 'I' & 'III'
CALL INTSCS(YPA,YPB,YRL,YRUP,YRIN,
1CPA,CPB,ALF,PHI,AA,YA,ZA,
2XB,YB,ZB,XAX,YAX,ZAX,XEX,YEX,ZEX,NX,NY)
ALF1=ALF(1)
ALF2=ALF(2)
PHI1=PHI(1)
PHI2=PHI(2)
C CALCULATES TWO ALF & PHI ANGLES FOR 'I' & 'III'
CALL INTSCS(XPA,XPB,XRL,XRUP,XRIN,
1CPA,CPC,PHI,ALF,XAX,YAX,ZAX,
2XAX,YAX,ZAX,XA,YA,ZA,XA,YA,ZA,NX,NY)
ALF3=ALF(1)
ALF4=ALF(2)
PHI3=PHI(1)
PHI4=PHI(2)
C SELECTS THE PROPER ALF & PHI ANGLES OUT OF THE FOUR VALUES
HALF=(ALF1+ALF2+ALF3+ALF4)-AMAX1(ALF1,ALF2,ALF3,
1ALF4)-AMIN1(ALF1,ALF2,ALF3,ALF4)/2
FPHI=(PHI1+PHI2+PHI3+PHI4)-AMAX1(PHI1,PHI2,PHI3,PHI4)
1-AMIN1(PHI1,PHI2,PHI3,PHI4)/2
900 WRITE(6,501) HALF,FPHI
901 FORMAT(' SELECTED',2F10.2)
C CALCULATES NEW PS FROM DATA OF POSITION D AND CORRECTS PT
ALFON=HALF-XPD
CALL INTPLT(XA,YA,ZA,ALFON,FPHI,NX,NY,CPO)
ALFON=HALF-XPC
CALL INTPLT(XA,YA,ZA,ALFON,FPHI,NX,NY,CPC)
905 WRITE(6,510) CPC,CPO
910 FORMAT(' NEW CPC & CPO CALLED',F15.5)
PSN=(PPC*CPO-PPD*CPC)/(CPC-CPO)
907 WRITE(6,511) HALF,FPHI,PST,PT
911 FORMAT(' ITERATION VALUES',2F6.2,2F10.2)
C CONVERGENCE TESTS
DELPS=PSN-PS
950 WRITE(6,552) PS,PSN,DELPS
951 FORMAT(' EPSPS VALUES',3F15.5)
952 EPSPS=ABS((PSN-PS)/PS)
WRITE(6,561) EPSPS
961 FORMAT(' EPSPS IS',F25.15)
EPSPSG=.0000000099*(PT**2.0)-.00000098*PT
IF(IEPS1.EQ.2) EPSPSG=.000000009*(PT**2.0)-.0000003*PT
IF(IEPS2.EQ.2) EPSPSG=.000000009*(PT**2.0)-.0000006*PT
IF(IEPS3.GT.EPSPSG) GO TO 310
GO TO 302
310 CONTINUE
IF(111.GT.10) GO TO 305
PS=PS+RELAPS*(PSN-PS)
PSC=PS
PST=PS
924 WRITE(6,525) PS

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INT01410
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INT02100

FILE: WVP FORTMAN PL

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525 FORMAT(' CURK PS IS ',F15.5)
GO TO 300
303 WRITE(5,171) FALF,FPP1,PS1,PT
171 FORMAT(' F15.2,F15.3)
GO TO 193
305 WRITE(6,307)
307 FORMAT(' SCANNED 100 TIMES')
GO TO 193
END
SUBROUTINE INTSCS(ARPI,ARP2,ARLO,ARUP,ARIN,
1HT1,HT2,RES1,RES2,X1,Y1,Z1,X2,Y2,Z2,X3,Y3,Z3,X4,Y4,Z4,M1,M2)
DIMENSION RES1(10),RES2(10),ARRES(10),A1(40),Y1(40),
1Z1(40),X2(40),Y2(40),Z2(40),X3(40),Y3(40),
2Z3(40),X4(40),Y4(40),Z4(40,40)
RES1(1)=9000.
RES1(2)=9000.
RES2(1)=9000.
RES2(2)=9000.
ISL=1
ISR=1
DAR=1.
AR2R=ARIN
GO TO 152
150 AR2R=AR2R+DAR
AR2RJ=AR2R
152 ARP1=AR2R-ARP1
ARP2=AR2R-ARP2
C CHECK FOR LOWER CALIBRATION RANGE
IF(ARP1.LT.ARL0) GO TO 150
IF(ARP2.LT.ARL0) GO TO 150
K=1
C CALCULATES INITIAL PENETRATION POINTS
CALL PENPTS(11,M2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJH=ARRES(2)
CALL PENPTS(11,M2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBJL=ARRES(1)
RBJR=ARRES(2)
C CALCULATES SUCCESSION PENETRATION POINTS
DO 140 I=1,1000
AR2R=AR2R+DAR
ARP1=AR2R-ARP1
ARP2=AR2R-ARP2
C CHECK FOR UPPER CALIBRATION RANGE
IF(ARP1.GT.ARUP) GO TO 195
IF(ARP2.GT.ARUP) GO TO 195
CALL PENPTS(11,M2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJH=ARRES(2)
CALL PENPTS(11,M2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBIL=ARRES(1)
RBIR=ARRES(2)
IF(RAJL.EQ.1000.) ISL=10
IF(RAJH.EQ.1000.) ISL=10
IF(RBJL.EQ.1000.) ISR=10
IF(RBJH.EQ.1000.) ISR=10
IF(RAIL.EQ.1000.) ISL=10
IF(RPIL.EQ.1000.) ISL=10
IF(RBIL.EQ.1000.) ISR=10
IF(RBIR.EQ.1000.) ISR=10
C CHECK FOR DIRECT HIT TO LEFT INTERSECTION,EVALUATE IF REQUIRED
IF(ISL.NE.10) GO TO 164
ISL=1
GO TO 183
164 IF(RAIL.NE.RBIL) GO TO 180
RES1(K)=RAJL
RES2(K)=AR2R
IF(K.EQ.2) GO TO 155
K=2

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INT02110
INT02120
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FILE: WVDR FORTRAN PI N P S

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      GO TO 183
C CHECK FOR INTERMEDIATE LEFT INTERSECTION, EVALUATE IF REQUIRED
180 IF (ISL.NE.10) GO TO 160
      ISL=1
      GO TO 183
160 IF ((FAJL-RBJL)/(FAAL-RBIL).GT.0.0) GO TO 183
      AA=(AF2RJ-AR2K)/(RAJL-RAIL)
      BA=AR2K-AA*RAIL
      AB=(AR2KJ-AR2K)/(RBJL-RBIL)
      BB=AR2K-AB*RBIL
      RES1(K)=(BB-BA)/(AA-AB)
      RES2(K)=AA*RES1(K)+BA
      IF (K.EQ.2) GO TO 155
      K=2
C CHECK FOR DIRECT HIT ON RIGHT INTERSECTION, EVALUATE IF REQUIRED
183 IF (ISR.NE.10) GO TO 161
      ISR=1
      GO TO 163
161 IF (RAIR.NE.RBIR) GO TO 182
      RES1(K)=RAIR
      RES2(K)=AR2K
      IF (K.EQ.2) GO TO 155
      K=2
      GO TO 163
C CHECK FOR INTERMEDIATE RIGHT INTERSECTION, EVALUATE IF REQUIRED
182 IF (ISR.NE.10) GO TO 162
      ISR=1
      GO TO 163
162 IF ((RAJR-RBJK)/(RAIR-RBIR).GT.0.0) GO TO 163
      AA=(AR2RJ-AR2K)/(RAJR-RAIR)
      BA=AR2R-AA*RAIR
      AB=(AR2RJ-AR2R)/(RBJR-RBIR)
      BB=AR2R-AB*RBIR
      RES1(K)=(BB-BA)/(AA-AB)
      RES2(K)=AA*RES1(K)+BA
      IF (K.EQ.2) GO TO 155
      K=2
C RE-INITIATE
163 AR2RJ=AR2R
      RAJL=RAIL
      RAJR=RAIR
      RBJL=RBIL
      RBJK=RBIR
140 CONTINUE
      WRITE(3,210)
210 FORMAT(' LOOP 140 THROUGH, NO POINTS FOUND')
      GO TO 155
195 IF (RES1(1).EQ.9000.0) GO TO 191
      IF (RES1(2).EQ.9000.0) GO TO 191
      IF (RES2(1).EQ.9000.0) GO TO 191
      IF (RES2(2).EQ.9000.0) GO TO 191
      GO TO 155
C EVALUATION OF INTERSECTIONS WHEN CURVES ARE ALMOST TANGENT
191 YGC=0.0
      CALL PENPTS(N2,N1,X3,Y3,Z3,HT1,YG0,APRES)
      R1=ABS(ARRES(2)-ARRES(1))/2
      CALL PENPTS(N2,N1,X4,Y4,Z4,HT2,YG0,APRES)
      R2=ABS(ARRES(2)-ARRES(1))/2
      RES2(1)=(X1**2)-(X2**2)+(ARP2**2)/(2.0*ARP2)
      RES2(2)=RES2(1)
      RES1(1)=SIGN(ABS((R1**2)-(RES2(1)**2)))
      RES1(2)=-RES1(1)
155 RETURN
      ENCL
      SUBROUTINE PENPTS(NX,NY,X,Y,Z,HT,YG,XR)
      DIMENSION Y(40),Z(40),Z(40,40),X(40),XR(10)
      IR=1
C SEARCH FOR J OF LOWER Y LINE
      DO 101 I=1,NY
      IF (Y(I).GE.YG) GO TO 102

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INT02810
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FILE: WVDR FORTRAN P1

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101 CONTINUE
102 J=J+1
C COARSE SCAN FOR ZERO PASS
C NEXT 4 LINES ARE EXECUTED IN FIRST SEARCH ONLY
YC=(Y(J+1)-Y(J))/((X(J+1)-X(J)))
ZX(1)=(Z(1,J+1)-Z(1,J))*YC+Z(1,J)
IF(ZX(1).EQ.HT) GO TO 107
103 CONTINUE
GO TO 116
C CALCULATION OF PENETRATIONS IN EITHER TRIANGLE
104 XM=(X(1)-X(1-1))*(Y(J+1)-Y(J))/(Y(J+1)-Y(J))
IF(ZM.EQ.HT) GO TO 105
IF((X(1)-HT)/(ZM-HT).LT.J.J) GO TO 105
DD=ABS(XM-ZM)+ABS(ZX(1-1)-HT)
XS=X(1-1)+(X4-A(1-1))*ABS(ZX(1-1)-HT)/DD
GO TO 110
105 XS=X+(X(1)-XM)*ABS(ZM-HT)/(ABS(ZM-HT)+ABS(ZX(1)-HT))
GO TO 110
C LOGICAL PENETRATIONS ACCUMULATION
107 XR(1)=A(1)
I=1
GO TO 113
108 XR(I)=X(I)
GO TO 111
110 XR(I)=XS
111 IF(IR.EQ.2) GO TO 114
113 IR=2
IR=I+1
GO TO 112
116 IF(IR.EQ.1) GO TO 117
XR(2)=1000.0
GO TO 114
117 XR(1)=1000.0
XR(2)=1000.0
114 RETURN
END
SUBROUTINE INTPLY(X,Y,Z,XS,YG,NX,NY,ZRES)
C LINEAR INTERPOLATION ON CALIPRATION SURFACE TO EVALUATE
C CP VALUE AT CO-ORDINATES XS,YG. THE RESULT RETURNED IS ZRES
C DIMENSION X(40),Y(40),Z(40,40)
C SEARCH FOR I OF LEFT X LINE
DO 1 JC=1,NX
IF(X(JC).GE.XG) GO TO 2
1 CONTINUE
I=JC-1
C SEARCH FOR J OF LOWER Y LINE
DO 3 JC=1,NY
IF(Y(JC).GE.YG) GO TO 4
3 CONTINUE
J=JC-1
AL=(Y(J+1)-Y(J))/(X(I+1)-X(I))
BL=Y(J)-AL*X(I)
YCR=(AL*XS)+BL
IF(YG.EQ.YCR) GO TO 7
IF(YG.GT.YCR) GO TO 5
C RESULTING Z IS IN LOWER TRIANGLE
X3=X(I+1)
Y3=Y(J)
Z3=Z(I+1,J)
GO TO 6
C RESULTING Z IS IN UPPER TRIANGLE
5 X3=X(I)
Y3=Y(J+1)
Z3=Z(I,J+1)

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INTC421J

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IN 7043 10
IN 7043 10

IN 704-50

INT0440
INT0440

INT(4410)

INT 04, 20
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IN: J443J
IN: J444J

INTC4440
INTC4450

INTC'446J

1:1 TC447C

INT 04483
INT 04480

INT 6449
INT 6450

INT 245 10

IN 704520

INTJ453J
INTJ454J

INT J 454 J
(INT C 455 J)

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